OPERATING INSTRUCTIONS

ALLIS-CHALMERS FUEL CELL POWER SYSTEM

(SYSTEM NUMBER 5R)

Prepared for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION MARSHALL SPACE FLIGHT CENTER Huntsville, Alabama

ALLIS-CHALMERS RESEARCH DIVISION

NASA Fuel Cell Systems Program Milwaukee, Wisconsin

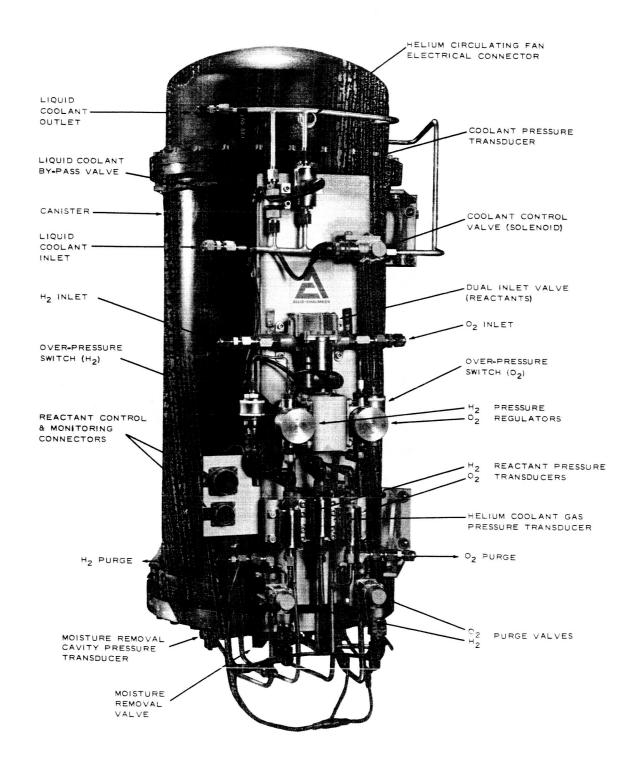


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SECTION I

SYSTEM DESCRIPTION

1.1 GENERAL DESCRIPTION OF OPEN LOOP FUEL CELL SYSTEM

The fuel cell system is an electro-chemical device in which the controlled temperature reaction of two input gases, hydrogen and oxygen, in the presence of a suitable electrolyte and electrodes, produces a direct current electrical output. The by-products of the reaction are heat and water which must be removed from the fuel cell. As the gases are consumed in the reaction, minute amounts of gas impurities (inerts) present in the reactant gases accumulate in the cell cavities. To maintain proper system performance, it is necessary to remove these impurities by periodically purging the cell cavities.

The basic operating voltage of the system is fixed by the number of cells, and the combination of electrical connections between the cells. Within the design limits, the load current will follow the demand, provided adequate amounts of reactant gases are supplied to the fuel cell.

This fuel cell is designated as an "asbestos capillary matrix" type in which the potassium hydroxide (KOH) electrolyte is held in a porous asbestos matrix without any circulation.

The by-product water is withdrawn from the fuel cell as vapor. It is produced at the hydrogen electrode, and diffuses into the moisture removal cavity through a KOH impregnated asbestos capillary matrix. The rate of water removal is controlled by maintaining the moisture removal cavity at a pressure equivalent to a predetermined electrolyte concentration. The quantity of water produced is proportional to the current produced by the fuel cell.

In the open loop system the moisture vapor, controlled by the moisture removal valve, is vented to a vacuum source.

Approximately one-third of the by-product heat is removed from the stack by evaporation of the product water. This helps promote good cell and stack temperature control. The majority of the by-product heat is removed from the fuel cell stack by recirculating helium gas over the finned edges of the cell plates. The heated helium gas then passes through a gas-toliquid heat exchanger where the excess heat is rejected to the liquid coolant after which it is recirculated. The liquid coolant is cooled externally of the fuel cell system. The helium gas is recirculated constantly at a fixed rate by fans and the amount of heat removed from the fuel cell is controlled by controlling the flow of the liquid coolant through the heat exchanger.

PERFORMANCE CAPABILITY GOALS

The performance capability goals of this fuel cell system are tabulated below:

2000 watts Nominal Power Rating

Overload 2700 watts (load profile)

Voltage Regulation 27 to 32.5 volts (22 volts min.)

Minimum Voltage (overload) 22 volts

195 ⁺ 5°F Cell Operating Temperature

Maximum Reactant Consumption Hydrogen - 0.22 pounds per hour

at 2000 watt load Oxygen - 1.75 pounds per hour

Reactant Inlet Pressure 175-400 psia 0 to 150°F Reactant Inlet Temperature

0.99998 hydrogen Desired Reactant Purity

0.999 min. 0.99995 oxygen

Thermal efficiency (min). 55%

Endurance 1250 Qualification Liquid Coolant

Liquid Coolant Supply
Liquid Coolant Pressure Drop
(max.)

60% methyl alcohol, 40% water by weight, plus corrosion inhibitors
120 pounds per hour at 60°F
15.0 psid

1.3 SYSTEM DIAGRAMS

1.3.1 Figure 1-1 illustrates schematically the complete functional fuel cell open-loop system. The basic input requirements to the open-loop cell assembly are:

Hydrogen Gas

Oxygen Gas

Auxiliary Power Supply for Start-up

Liquid Coolant

Vacuum

Helium Gas

The products removed from the fuel cell assembly are:

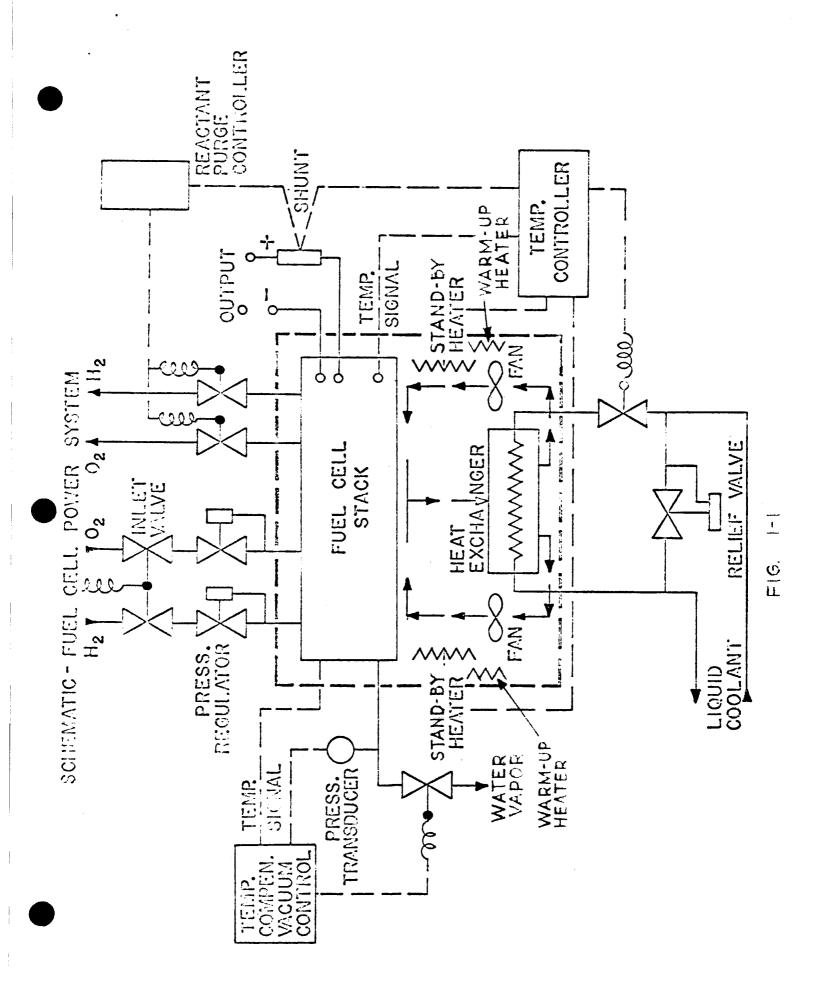
Direct Current Electricity

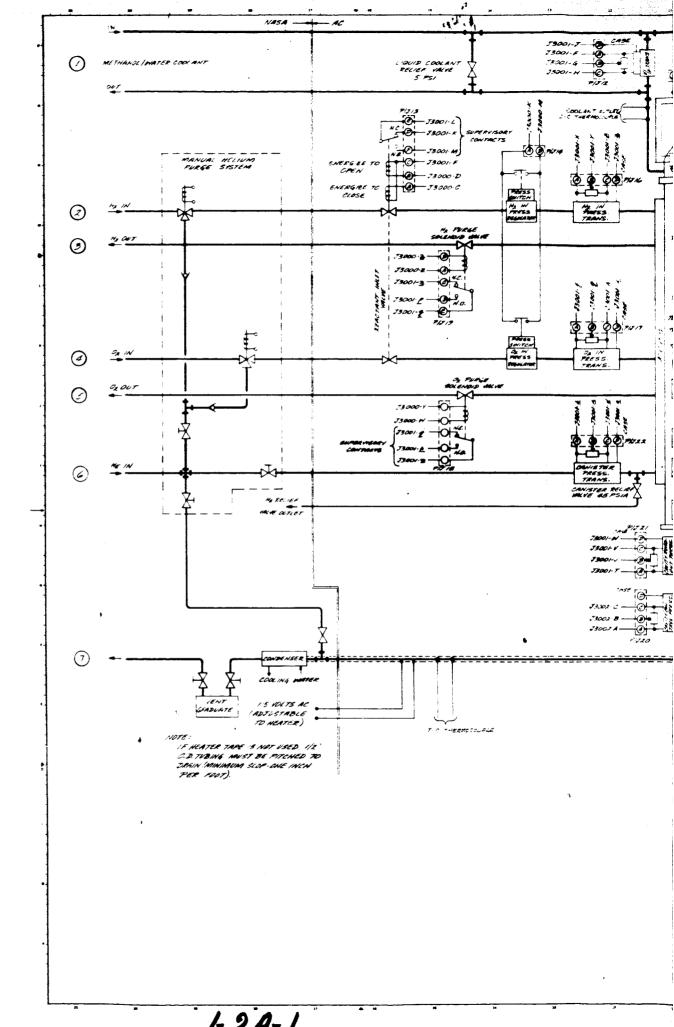
Water

Heat

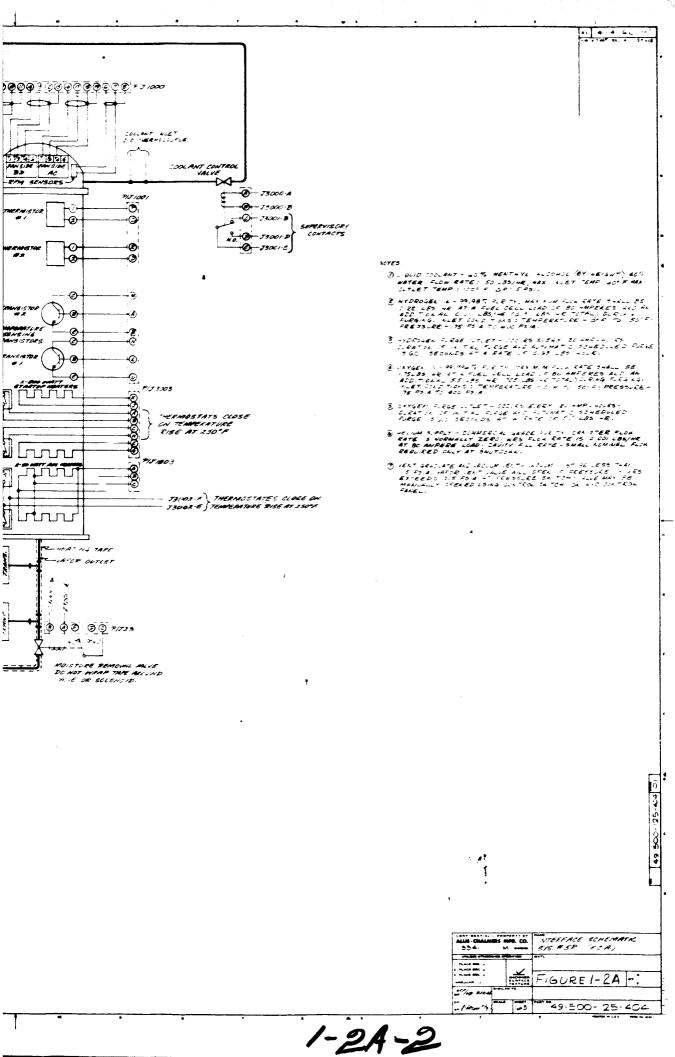
The specifications for each of the input and output items are detailed in Section 2.1 Fuel Cell Assembly and Section III - INTEGRATED SYSTEM OPERATIONS.

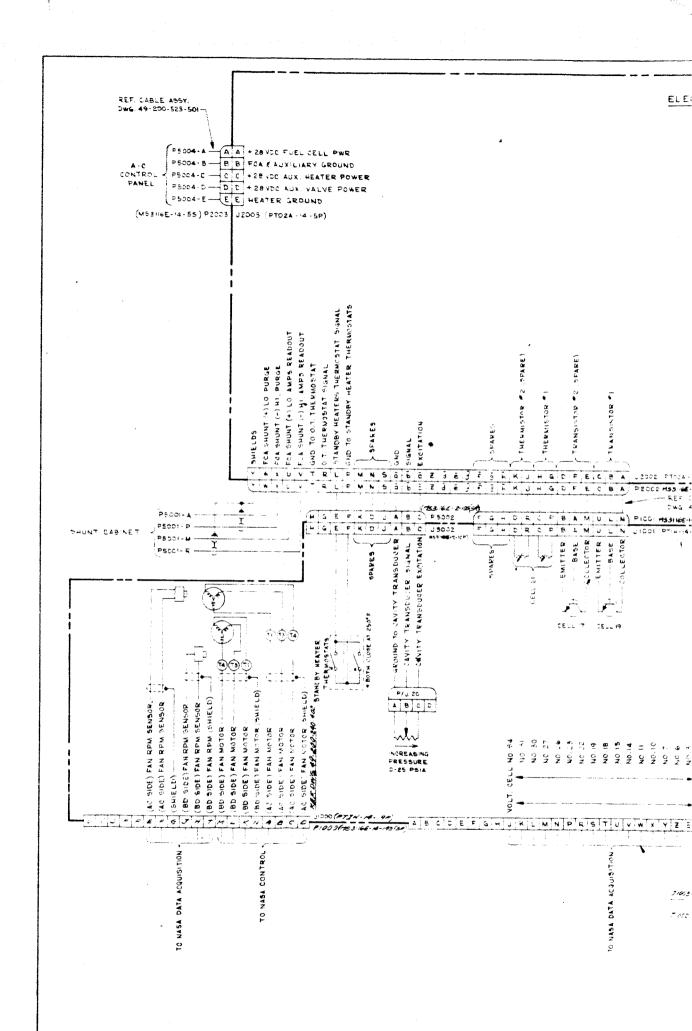
1.3.2 Figure 1-2A, 1-2B and 1-2C (Drawing No. 49-500-125-404) is the Fuel Cell System Schematic illustrating SYSTEM OPERATIONS. A description of the subsystems if found in Section 4.

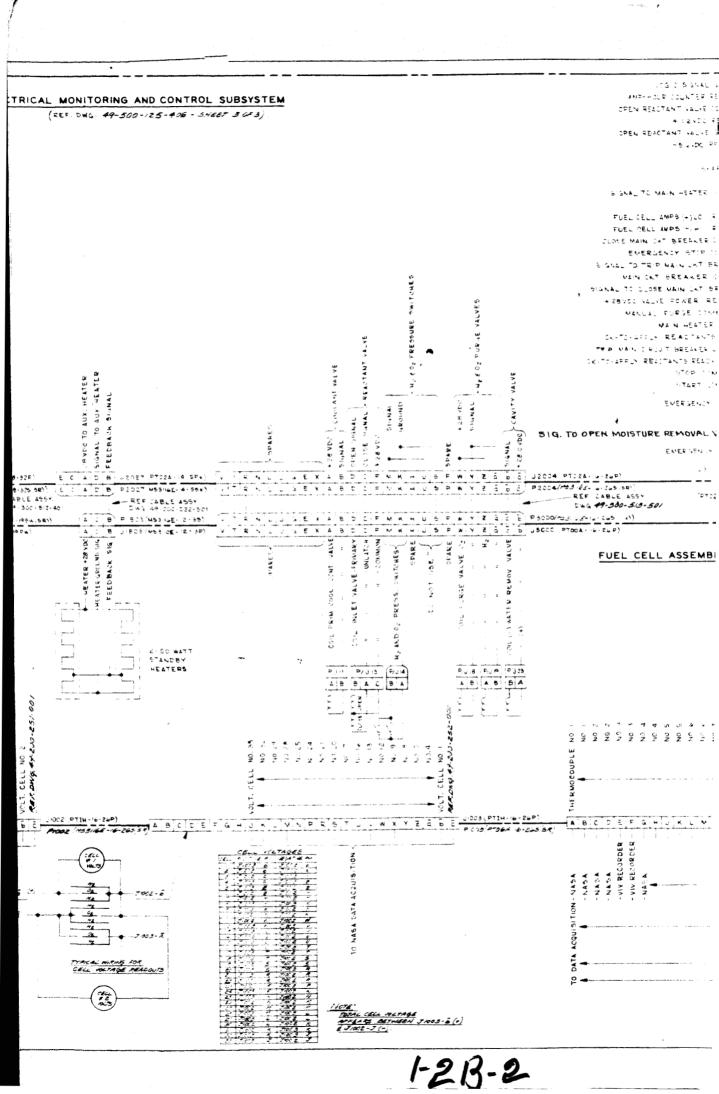


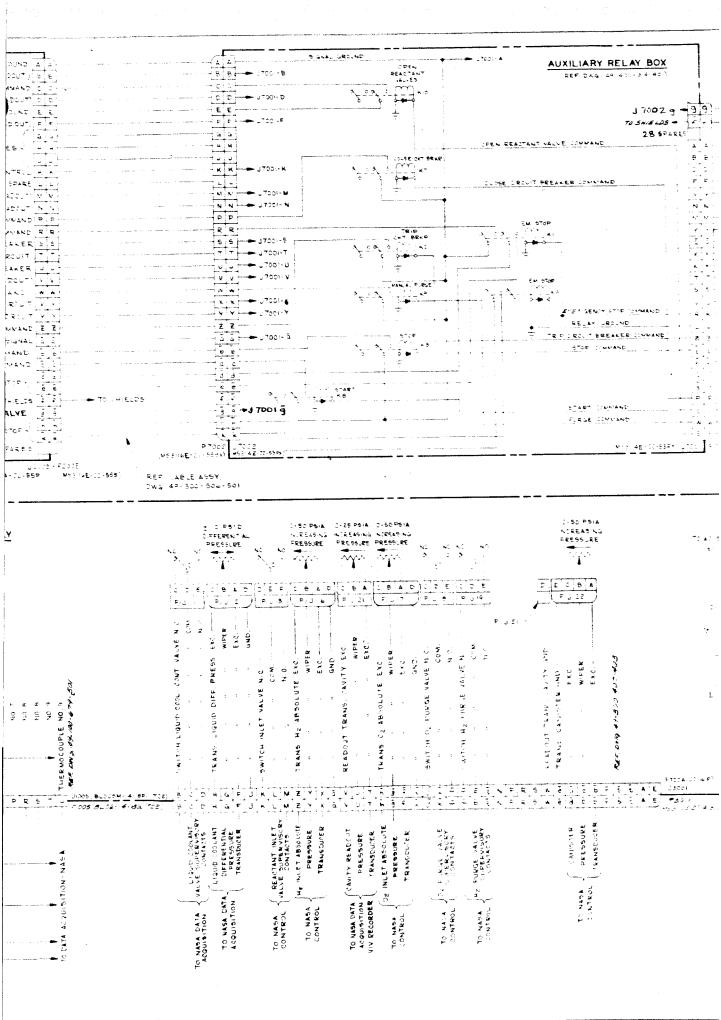


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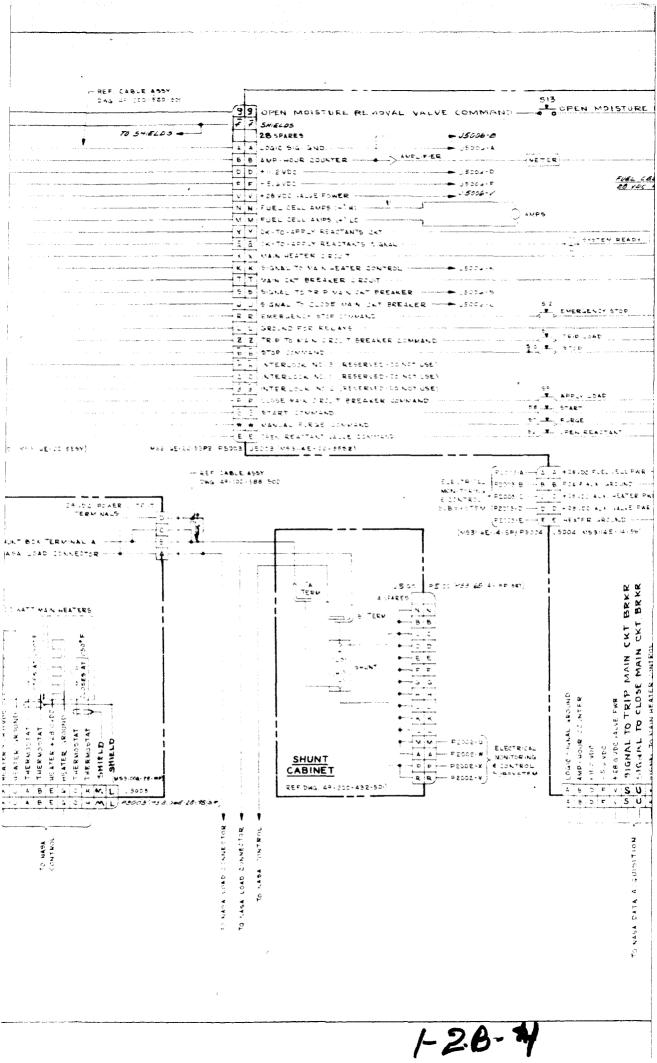


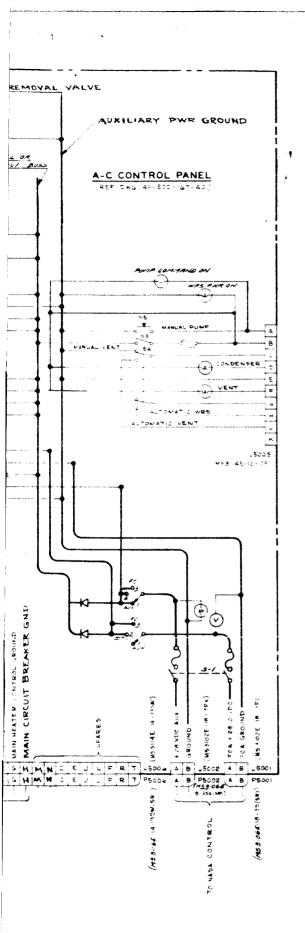






1-2B-3





ON AC CONTROL PANEL
REMOVED WIRES CONNECT
J5003M TO J5006M
J5003M TO J5006M
J5003M TO J5006M
ADDED 9 TO PYJ5003
FOLLOWING LAMPSPUMP COMMAND ON
CONDENSER
VENT
ALL HAD BEEN
CONNECTED DIRECTLY
TO FUEL CELL OR
28 V.DC AUX. BUSS
INSTEAD OF THRU
S3 AND FUSE.
SYSTEM READY LIGHT
DISCONNECTED FROM
FUEL CELL OR 28 V.D.C
AUX. BUSS AND AUX.
POWER GROUND.
ON FUEL CELL ASSEMBLY
TERMINAL M AND L
ADDED TO J 3003
ALONG WITH SHIELDS

01 3-22-66

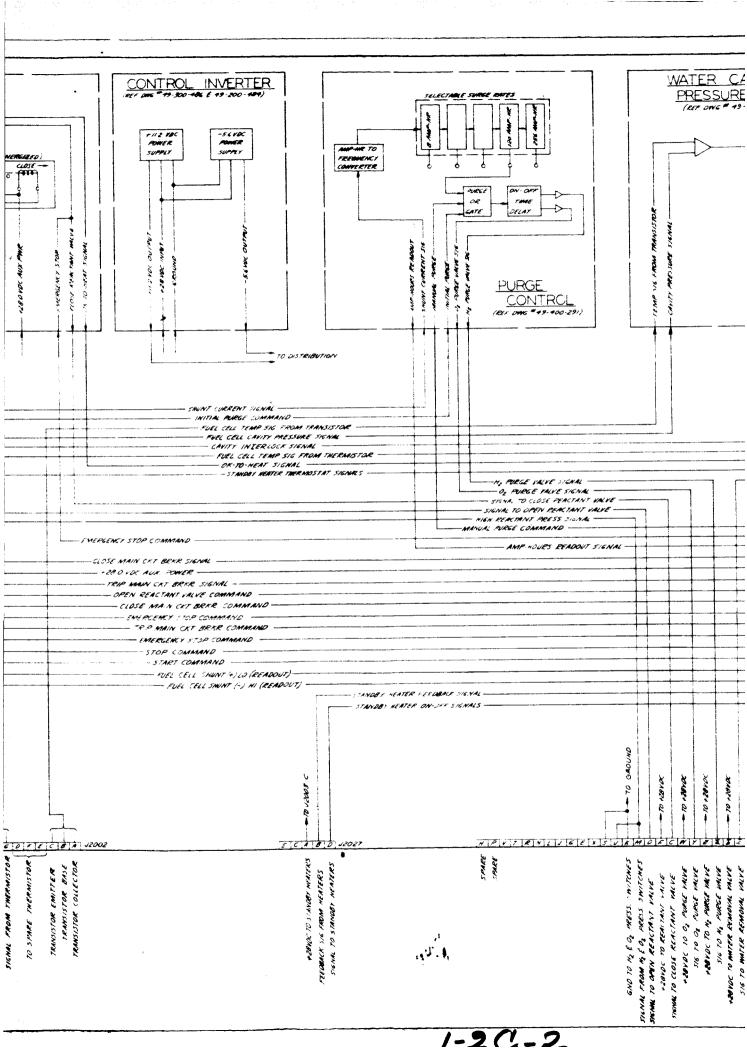
02 6-3-66 9 4 8.

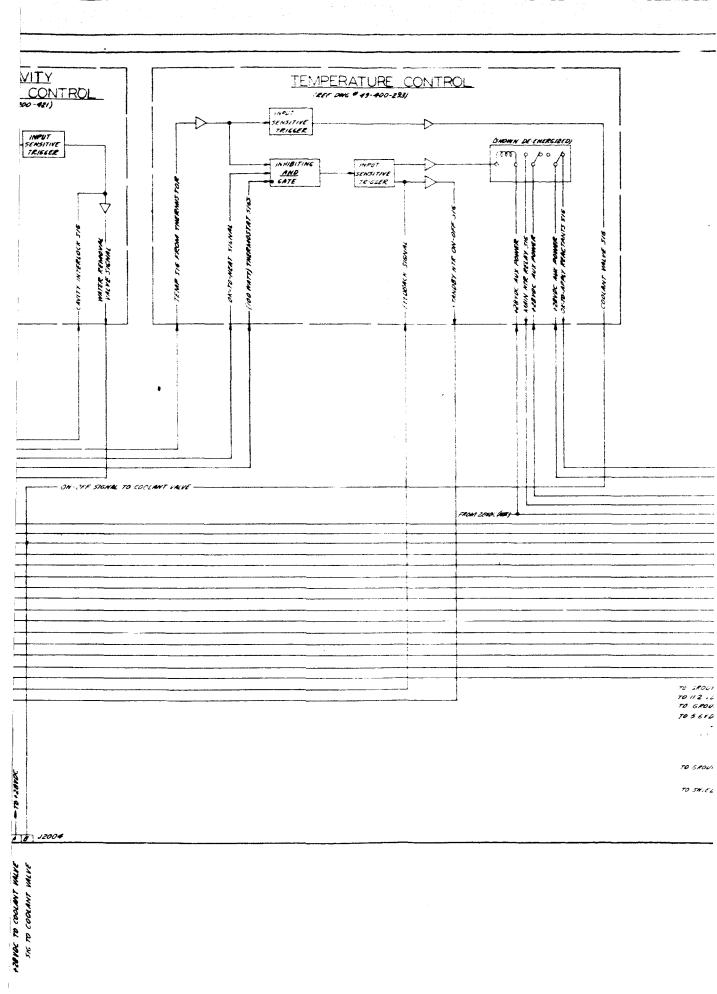
REDUCED REPRODUCTION OF 49-500-125-404 SHEET 2 OF 3

ALIS CHALME			CELL S.		
P. OL S. DEL.	 ;				
25 4746	- 2~3	Fig	1 - 2	В	

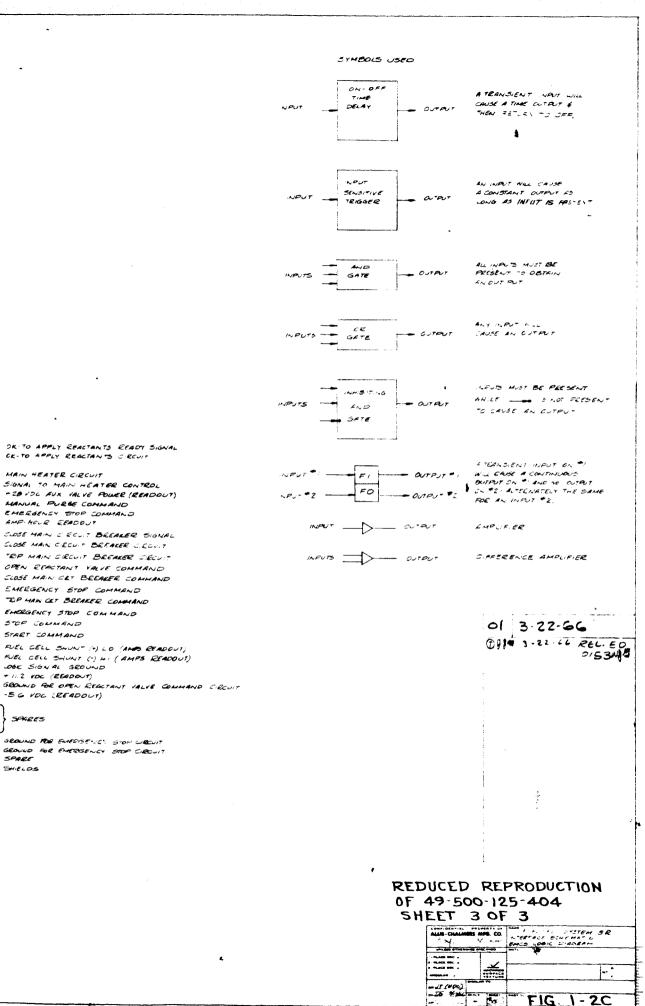
1-28-5

START AND GATE YOUTAGE FLOSS REMOVE LOAD OR GATE STOP OR GATE TRIP MAIN CAT BREER-EMERGENCY STOP FUEL CELL +28VDC <28 V DC -CLOSE MAIN CAT BRKR TRIP MAIN CKT BRKE MASTER
CONTROL
(REF DING #49-300-174) +28Y DC FUEL CELL POWER F1: £ AUX PWR GROUND +28YDC AUX HEATER POWER +28YDC AUX VALVE POWER HEATER GROUND FULL CELL SHUNT (1) LO SIG FUEL CELL SHUNT (1) NO SIG FC SHUNT (1) LO - AMPS READOUT FC SHUNT (1) NI - AMPS READOUT SPARE SPARE SPARE SPARE THERMISTOR SPARE SPARE SPARE THERMSTATS SPARE GROWND TO CAVITY TRANSOUCER CAVITY PRESSURE SSENAL EXCITATION TO CAVITY TRANSDUCER 1-2 (-1





1-91-2



DK-TO APPLY REACTANTS READY SIGNAL CK-TO APPLY REACTANTS CROUT

SIGNAL TO MAIN HEATER CONTROL +28 VOC AUX VALVE POWER (READOUT)

SLOSE MAIN & ROUT BREAKER SIGNAL CLOSE MAIN CIECUIT BREAKER CLECUIT

TOP MAIN SIRCUIT BREAKER SIRCUIT

OPEN REACTANT VALVE COMMAND

CLOSE MAIN CLY BREAKER COMMAND EMERGENCY STOF COMMAND TEP HAIN OUT BREAKER COMMAND

FUEL CELL SHUNT (+) LO (AMS READOUT)

GROUND FOR EMEDIFIED STON WECUIT GROUND FOR EMERGENCY STOP CHECUIT

FUEL CELL SHUNT (-) HI (AMPS READOUT)

MAIN HEATER CIRCUIT

MANUAL PURSE COMMAND

EMERGENCY STOP COMMAND AMP HOLR EFADOUT

EMERGENCY STOP COMMAND

STOP COMMAND

START COMMAND

JOHE SIGNAL GROUND + 11.2 VOC (READOUT)

-5 6 VDC (READOUT)

SPARES

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SECTION II

INSTALLATION INSTRUCTIONS

2.1 UNPACKING, INSPECTION AND ASSEMBLY

2.1.1 Shipping Containers

The fuel cell module including the reactant control valve assembly will be shipped within a wooden container as shown in Figure 2-1 (drawing No. 49-400-230-401). The fuel cell module has been pressurized with helium to a pressure of approximately 5 psig and appropriate care should be exercized in handling the unit. The shipping container should be placed in the proper vertical attitude to facilitate cell removal.

The fuel cell module should be supported from the eyelets provided in the upper clamp-ring shim, and then it may be unbolted from the shipping container and moved to the test area.

The other items supplied by Allis-Chalmers for the assembly of Fuel Cell System #5R will be boxed in wood and/or cardboard containers suitably protected against moisture and dirt.

2.1.2 Inspection Prior to Assembly

All major components have been cleaned and packaged at the Allis-Chalmers facility, however, prior to assembly all components should be examined for cleanliness.

2.1.3 Assembly of the Fuel Cell System

Fuel Cell System#5R as delivered consists of five major subassemblies to which interconnections must be made in the field. Refer to Figure 2-2A (Drawing No. 49-400-250-405 and Figure 2-2B (Drawing No. 49-200-431-504.

These figures physically locate each point of interconnection, identify the interconnecting cable, show the connector designation and specify the customer tie-in points. The major subassemblies are:

- Item 2 Fuel Cell Module whose Major Subassemblies are Stack the Fuel Cell and the Reactant Control Subsystem.
- Item 4 Electrical Monitoring and Control Subsystem.
- Item 5 Current Shunt Cabinet
- Item 6 Allis-Chalmers Auxiliary Relay Box (For reference only)
- Item 7 Allis-Chalmers Control Panel (For reference only)

Allis-Chalmers has furnished interconnecting electrical cables between the fuel cell module and the EMCS, the module and the shunt cabinet and a "Y" cable from the EMCS to the shunt cabinet and from the EMCS to the fuel cell module.

In addition, Allis-Chalmers has furnished all mating connectors for the remaining electrical connectors and all pneumatic/hydraulic fittings for use on the A-C furnished equipments.

2.1.4 Equipment Furnished by the Marshall Space Flight Center

MSFC will furnish the following major items for the test setup of System #5R.

A. All operational controls including switches and indicators. Figure 2-3 contains a listing of the recommended controls and indicators for operation of the test setup. Figure 2-4A (Dwg. No. 49-200-550-501),

Figure 2-4B (Dwg. No. 49-400-318-401),

Figure 2-4C (Dwg. No. 49-400-314-401).

Figure 2-5 (Dwg. No. 49-200-523-501),

Figure 2-6 (Dwg. No. 49-300-506-501).

Figure 2-7 (Dwg. No. 49-300-520-501).

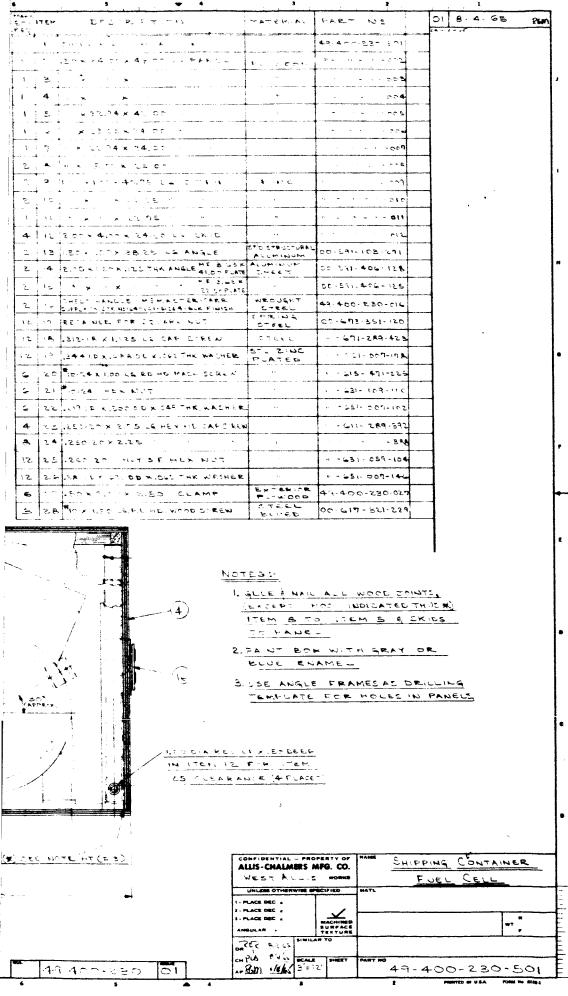
Figure 3-4 (Dwg. No. 49-400-349-402)

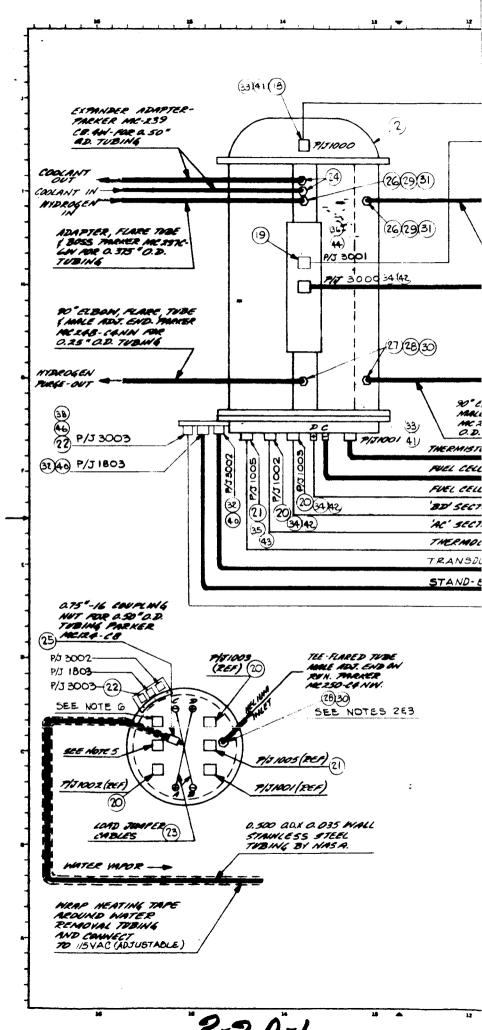
contain additional information on the method of control and indicator hookup.

B. All tubing, valves, gases, and flowmeters required to bring the reactant gases, helium gas and the liquid coolant to the fuel cell interface and to handle the by-product water. Figure 1-2A (Dwg. No. 49-500-125-404).

13 41.95 24.75 12.00 8 -0127 .015 CA (E. ... THE 5 8 \$14 FOR TEN (CHACEL FE DOV THIS SIGE UP 6 13, i 12.25 (<u>a</u>) * DEE 150 1

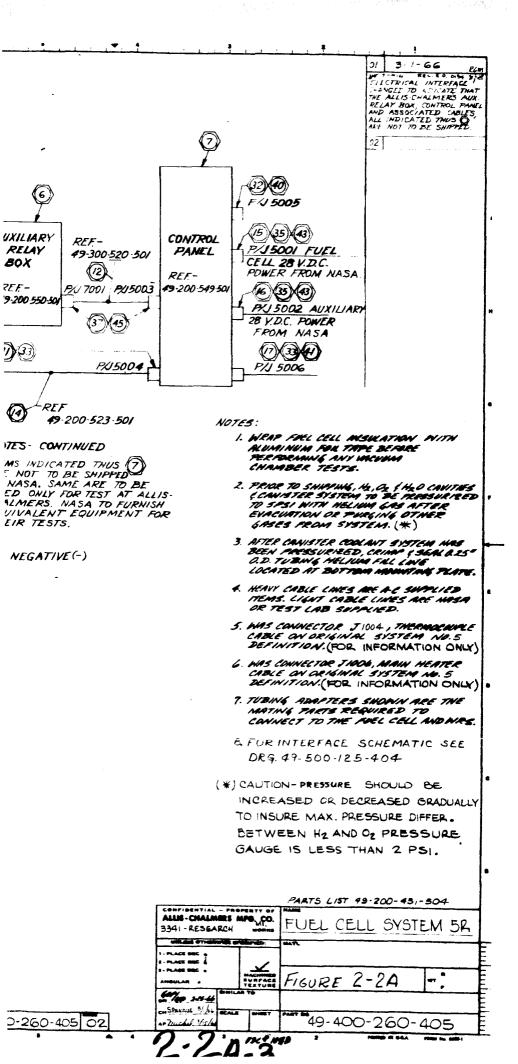
<u>, por service.</u> ENGLANCE NO. 22.74 11.4 DETAIL IL HC-E BUTTALLEY BY THE FORM 15 GLUE TO SETHER <u>", ~ , R.E.F.</u>.. AND THE STATE OF T 9.12 51 1 1.25 11





2-2A-1

FAN POWER & RPM SIGNALS PRESSURE TRANSDUCER & SUPERVISORY CONTACTS - OXYGEN IN 34)42 ADAPTER, FLARED TUBE & BOSS. PARKER MC237C-UM FOR O. 315" O.D. TUBING. REF -49-300 506 54 ELECTRICAL (35)(43) Œ MONITORING AND PXI 2005 (9) LALVE POWER PN-2004 CONTROL SUB-SYSTEM PX17002 14J 2002 (4)37**/4**5) P/J 2027 P/J 2003 - OXYGEN PURGE-OUT 'BON FLARED TUBE {
' ADT. END. TARKER
' BO-CANN FOR 0.25"
TUBING. (33)(4) P/J 5100 CURRENT E SIGNALS (10) SHUNT NEGATIVE (-) TERMINAL (1) CABINET A POSITIVE (+) TERMINAL ON CELL VOLTAGES ON CELL VOLTAGES OUPLE CABLE (BD SIDE) FUEL C TERMI CER SIGNALS(10) Y HEATER POWER **(8**) MAIN HEATER POWER ALLIS CHALMERS -- NASA ELECTRICAL INTER-FACE ę



1			6
	P		
REQ.	ITEM	DESCRIPTION	PART NUMBER
-	_	Finel Cell System #5R PIX	149-400-260-405
-	^	Firel Cell Assembly	49-500-105-510
-	~	Intentace Schematic	49-500-125-404
<u> </u>	\	Flactuical Monitoring and Control Subsvetem (EMCS)	49-200-585-502
1	H 4		49-200-432-501
-	1	Auxiliary Relay Box DO NOT SHIP - USE FOR 49-200-550-501	49-200-550-501
-	2		49-200-549-501
	_ α	Cable Stand-by Heater Power	49-200-522-501
-	0	Cable RCAS to FMCS Valves	49-300-513-501
	10	Cable. EMCS to Thermistors, Shunt Cab, and Transducers	49-100-706-501
-	12		49-100-588-502
	12	Aux. Relay Box to Control Panel	49-300-520-501/
-	13	1	49-300-506-501
_	14	EMCS to Control Panel .	49-200-523-501
-	15	al Connector (P 5001)	MS316E-18-3S(SR)
-	16	Electrical Connector (P5002)	MS316E-18-35x (SR)
ţ	17	Flectrical Connector (P5006)	MS316E-14-19 SW (SR)
	1.0	The talent Connector (D1000) Bandiv	PT06A-14-195(SR)

	19	Electrical Connector (P3001)	MS316E-20-415 (SR)
2	20	Electrical Connector (P1002-P1003)	MS3116E-16-26S'(SR)
-	,	Connector	BL06-14-18S-TC2
_	2.2	•	. MS3106E-28-198 (SR)
2	23	Load Jumper Cable	49-100-588-501
,	2.4	Plug. Aluminum (Parker)	4-PNTX-D
_	25	Cap. Gres. (Parker)	8-FNTX-SS
-	26	1	6-FNTX-SS
2	2.7	Cap. Cres. (Parker)	4-FNTX-SS
	28	Not Compling Gree. (Parker)	PAH-124-C4W
2	2.0	Coupling Cres.	PAH-124-C6₩
-5	30	(Parke	PAH-125-C4
~ 2.B	31	Sleeve, Cres. (Parker)	PAH-125-C6
	32	tacle	MS3181-12N
2	.33	Elec. Conn.	MS3181-14N
វ	34	Elec. Conn. Receptacle	MS3181-16N
4	35	Cap. Elec. Conn. Receptacle SHIP 2 ONLY (NSED FOR TEST BUT NOT	SHIPPED MS3181-18N
E	36	Can. Elec. Conn.	MS3181-20N
4	137	Elec. Conn.	MS3181-22N
-	38		10-70500-28
1	39		
7.3	40	Cap. Elec. Conn. Plug	MS3180-12C
	- F		MS3180-14C

Z.	42	Cap. Elec. Conn. Plug		MS3180-16C	
4	43	Elec. Conn.		MS3180-18C	
	44	Cap, Elec, Conn. Plus		MS3180-20C	1
4	45		P I ONLY (REMAINING B ON APPARATUS	PED MS3180-22C	
	46		(Bendix)	10-70506-28	
	47				
	48	Shiming Container		49=400-230-501	
REF	* 49	End Item Configuration Control	rol	49-300-488-401	
•	Ą				
,	,	• 1			
					.07
01	3-10-66	66 Rm 04	UNLESS OTHERWISE NOTED ANGLES & OMERSIONS ARE IN INCHES & ANGLES & MACHINING TOLERANGES ARE:		
6	AND PARTY SAME		DIMENSIONS UP TO 8 INCL. DVER \$ TO 84 INCL. OVER 24	FUEL CELL SYSTEM	
19067	Brus	10000 Ann (2) 10 U. W. A.L.	FRACTIONAL & T	No. 5E (Parts List)	
1	1.600	RELIGIOUS CONTRACTOR OF THE PROPERTY OF THE PR	DECIMAL #		*
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TOT	DO NO.	2300	RESERREN - BASIL	PIGNETO FISHER CALE	18
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33.	35.41	AWDAS.	The	04-11-200-431-504	
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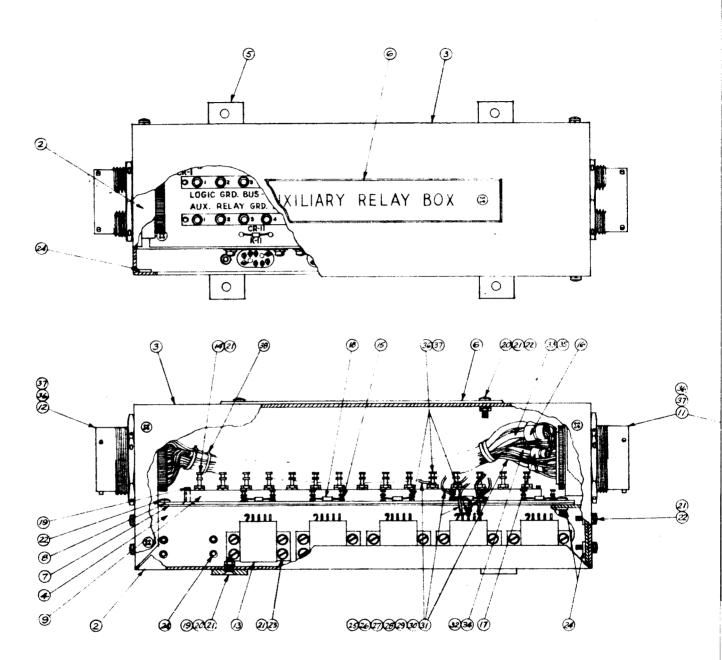
RECOMMENDED SYSTEM #5R CONTROLS AND MONITOR LIGHTS

Supp	ort	Light Monitor
1.	Helium purge - valve control (switch)	x (open)
2.	115 Vac power (switch)	x (on)
3.	28 Vac auxiliary power (switch)	x (on)
4.	Fan power (switch)	x (on)
5.	WRS heater tape (switch)	x (on)
6.	Vacuum pump - 1.5 psia (switch)	x (on)
7.	Vacuum pump - reference vacuum (switch)	x (on)
8.	Coolant pump (switch)	x (on)
9.	Stack heater power (switch) 1600 watt should have circuit for thermostat	x (on)

	MEQ.	ITEM	DESCRIPTION	MATERIAL	
	X		AUXILIARY RELAY BOX ASSEMBLY (PIX)		49-400-318-401
	\	N	BOX	6061-74 4UM 49-300-555-00	9-300-555-001
*	\	W)	CONER	6061-74 ALUM 49-300-556-601	9-300-556-601
A	\	4	CHANNEL	6061-74 MIUM 49-300-557-001	3-300-557-001
	0	5	MOUNTING PLATE	6061-T4 ALUM 49-100-768-001	3-100-768-001
	\	0	NAME PLATE	.06 LAWICOLD 49-100-770-001	1-100-170-001
7	\	1	INSULATOR BUNRD	.0316485 GANGER 49-100-771-001	9-100-771-001
- (00	CIRCUIT BOARD	100-809-002-64 MANASSESSESSESSESSESSESSESSESSESSESSESSESSE	3-200-608-001
1-1	N	0	BUS BAR	BRASS 45	49-200-606-001
}	X	9	SCHEMATIC WIRING DIAGRAM		49-400-314-401
7	\	>	CONNECTOR	MS	MS3114E22-55PY
8	\	12		M	MS314E22-55PX
	N	2	RELAY DPDT, 24 VDC POTTER & BRUMFIELD SCIIDB	3t	49-200-550-013
	30	14	TEKNIMAL, SOLDER, CAMBION TYPE 2051-1	5 /	49-200-550-014
	S	3	11 1 VECTOR T-13	*	49-200-550-015
	4	10	CINIMING INSULATED BURNEY YEC-180	W	MS25311-180
	4	1			MS25311-110
	1	8)	SILICON RECTIFIER MOTOROLA IN4003	*	49-200-550-018
	B	0	MACHINE SCREW SALADA 37 FIT-40 CO-1850	SW	11524692- AN

6 20 NUT. HEX 44-40		11	44-40								NAS671C-4	-
27	_	YER, SP217.#4	17#4						-		MS35338-78	
22	. MACHINE SCREW, PANTID CROSS.	REW PANTO CROSS	HD, CRUSS	1 12	P. S.	44.40.	r.37			"	MS51957-15	
44 23 MACHINE SCKEN, FIL-HD, #4-40 x.31		X6W, FILHD, #4-40	HD,#4-40	7	7 × . 3.	~				"	ANSOOD4-5	
24	1	T, #4-40, PENW	40, PENN		ENGE	2,54	5-27-40-5	2			49-200-550-024	
25	1	X, UNSHIELDED, B-	1 DED B		20(19)	132), 14	M MA	161/2	CKAR 2		49-200-550-025	1
26	1	"					27		6		49-200-550-026	
FT 27 " Exams, "	`	" /A			2.0	~		14	7		49-200-550-027	
288 "		" //	"	1 1	, , ,		,,	•	. 4		49-200-550-028	
29 "	*	E & RED , "				ونو	11	**	2/ //		49-200-550-029	1 <u>.</u> :
30		Sauce "	, g				77	7. 1	5/ '		49-200-550030	
1 2 1 " " \$ YELLOW! "	"	\$ YELLOW! "	*	1	,		, ,	11	14		49-200-550-031	
1 ST TUBULAR BRAID, 078 1.D.	TUBULAR ERAID, 078			, ·)	1.D. ALPHA#		2163	11011	10 IN. LG.		QQ-8-575	
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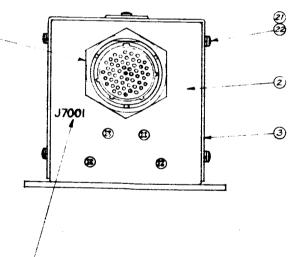


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NOTES:

- I. FOR SCHEMATIC WIRING DIAGRAM, SEE DRAWING 49-400-314-401.

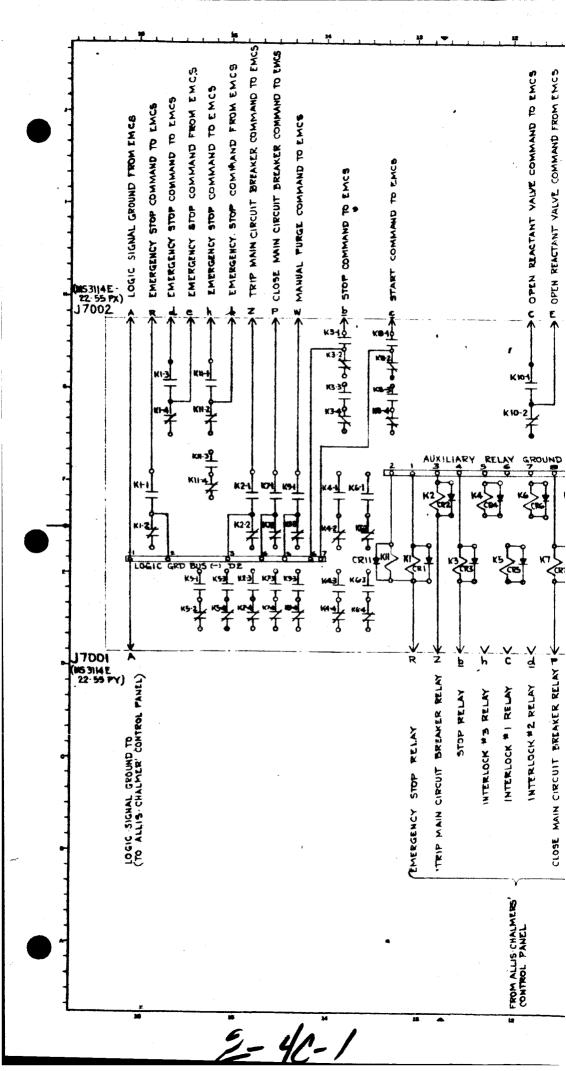
- 2.50LDER WHERE REQUIRED PER NPC-200-4.
 3. HEAT CHRINK TUBING PER MSFC-PROC 273.
 A. ROUTING, LACING, ETC. PER ELECTRICAL FABRICATION PROCEDURE MSFC-PROC-256.
 5. CHECK FOR CONTINUITY PER SCHEMATIC.



RUBBER STAMP CONNECTOR IDENTIFICATION NUMBERS IN WHITE, . 19 HIGH. "JTOO!" ON SAME END AS ITEM(1), "JTOO2" ON OPPOSITE END

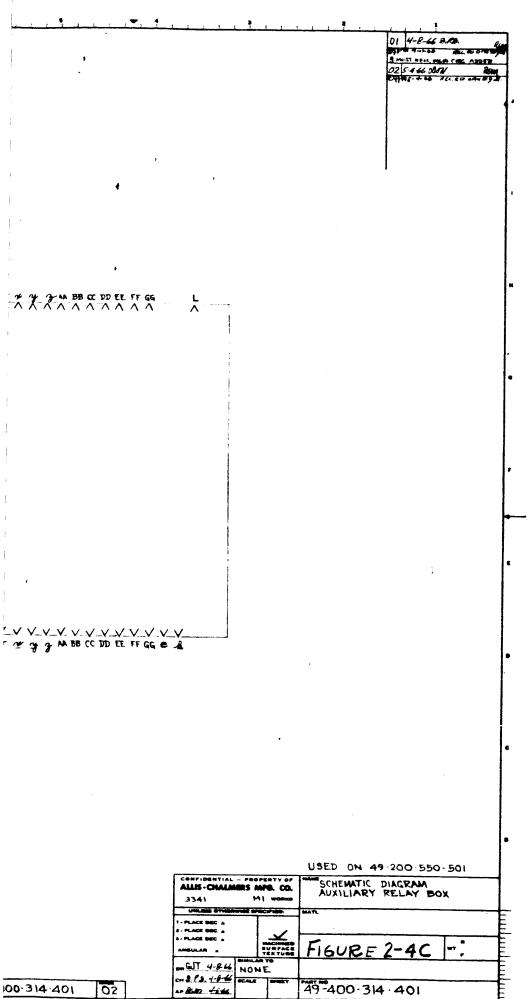
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DSH 4-944 PAT 1:016 REID J. HALL FULL	L /~/	49-400-3/8-40/

49-400-318-401 01



OK TO APPLY REACTANTS READY SIGNAL FROM EMCS YO SIGNAL TO TRIP MAIN CIRCUIT BREAKER FROM EMCS SIGNAL TO MAIN HEATER CONTROL FROM EMCS FUEL CELL AMPS (+) LOW (READOUT) FROM EMCS ACT SIGNAL TO CLOSE MAIN CIRCUIT BREAKER FROM EMCS FUEL CELL AMPS (-) HI (READOUT) FROM EMCS +28 YOLT DO VALVE POWER (READOUT) FROM EMCS AMP. HOUR COUNTER (READOUT) FROM EMCS -BIG VOLT D.C. (READOUT) FROM EMCS + 11.2 VOLT D.C. (READOUT) FROM EMCS OK TO APPLY REACTANTS CIRCUIT TO EMCS SIGNAL TO OPEN MOISTURE REMOVAL VALVE TO EMCS WIT MAIN CIRCUIT BREAKER CIRCUIT TO EMCS MAIN HEATER CIRCUIT TO EMCS × E MANUAL PURGE RELAY & AUXILIARY RELAY GROUND I START RELAY IN TO ALLIS CHALMERS' CONTROL PANEL FROM ALLIS CHALMERS' CONTROL PANEL TO ALLIS CHALMERS' CONTROL PANEL SHIELD FROM ALLIS CHALMERS' CONTROL PANEL TO ALLIS CHALMERS' CONTROL PANEL TO ALLIS CHALMERS' CONTROL PANEL OPEN REACTANT VALVE TROM ALLIS CHALMERS' CONTROL PANEL FROM ALLIS - CHALMERS' CONTROL PANEL TO ALLIS CHALMERS CONTROL PANEL FROM ALLIS-CHALMERS' CONTROL.

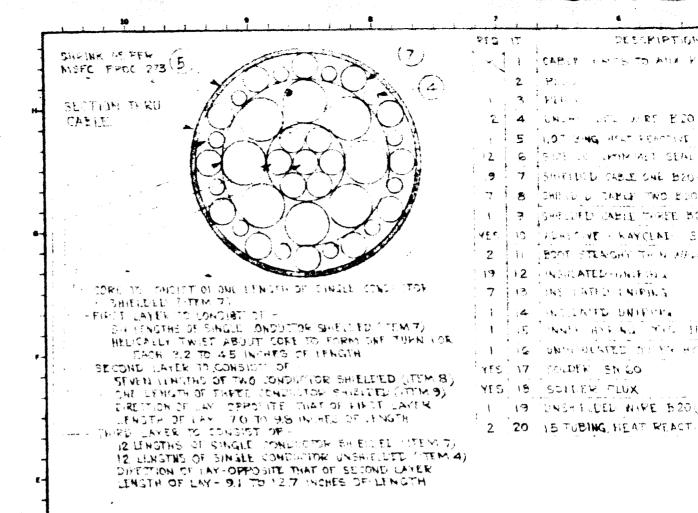
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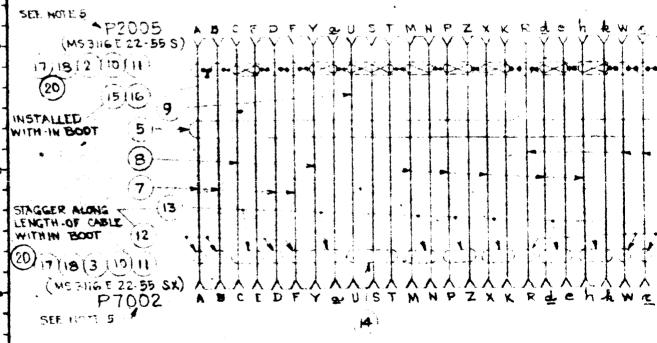


NOTE ! REQ IT. I EACH WIRE MUST BE CHECKED FOR ELECTRICAL CONTINUITY CABLE, . ١ PER WIRING DIAGRAM. NOTE 2 ١ PLUG 2 EACH WIRE MUST BE CHECKED ı 3 PLUG FOR INSULATION RESISTANCE TO EACH OTHER WIRE, THE 5 4 UNSHIELDE INSULATION RESISTANCE 5 .38 TUBING SHALL EXCEED 50 MEGOHMS AT 500 VOLTS 2 6 BOOT STR D.C. NOTE 3 7 YES ADHESIVE SOLDER AS PER NPC 2004 YES 8 SOLDER 9 YES SOLDER (10) 9 (8) 7 (6) 2 2 10 38 TUBING P 2003 BDC (MS 3116E14-55) A SHRINK AS PER MSFC-PROC-273 16'0 OVERALLLE (3) P5004 (MS 3116 E14-5 2) P2003 EN P5004 EN 49 125-1

ESCRIPTION	MATER
MCS TO CONTROL PANEL	
D WIRE BIG (19/29) 600V- 18 FT LG.	
, HEAT REACTIVE (MSFC-276) 18 FT LG.	276-31BK0
NIGHT THIN WALL 202 AD 42-3	
- RAYCLAD 5-1006	
SN 60	QQ -S-5 TYPE RA
FLUX	MIL- F-142 TYPE A
HEAT REACTIVE (MSFC 276) 1.0 IN.LG	276-31BKO
RUBBER STAMP. OR S NUMBERS (P2003 A CONNECTORS USING SIMILARLY APPLY MIDWAY BETWEEN	IND P500 G CHARAC "PART N
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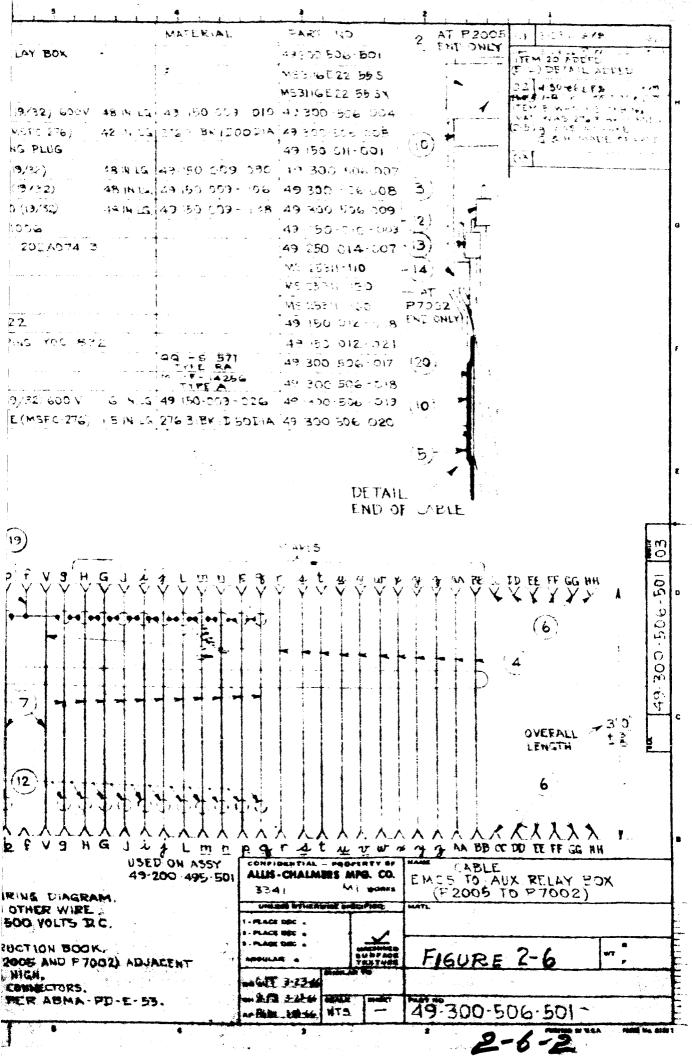
3-23-66 D.R.D. IAL PART NO. cand 3-23-44 2) REC.ED 144 1842 ITEM 5 VIAS . SO TUBING 49-200-523-501 276-31 BK OD 50 DIA. IT TO ADDED A-4) DETAIL ADDED MS 3116 E14 - 55 02 4-30-46 S.P.S. Rem MS 3116 E14-5P CITAL S-1-ES PELES OF THE PER 3-013 49-200-523-004 D38DIA 49-200-523-005 49-250-014-004 49-150-010-003 H 49-200523-008 56 49-200-523-009)38DIA 49.200.523:010 ONNECTOR IDENTIFICATION 4) ADJACENT RESPECTIVE TERS APPROXIMATELY . 12 HIGH 0.49-200-523-501 DRS. FORM ONE TURN FOR 4 EACH I.G TO 2.2 INCHES OF LENGTH, DIRECTION OF LAY TO BE THE SAME FOR POTH CAPLES DVE TWO CABLES TO FORM AS INCHES. DIRECTION OF DUAL CABLES. USED ON ASSY 49-200-495-501 CONFIDENTIAL-PROPERTY OF CABLE ALLIS-CHALMERS MPG. CO. EMCS TO CONTROL PANEL P2003 TO P5004 UNLESS OTHERWISE SPECIFIED: S-PLACE DEC ± HPLACE DEC ± FIGURE 2-5 OF GUT 3-23-64 CHARS 3-23-66 SCALE SHEET PART NO. AP REM SHALL NTS 49-200-523-PRINTED IN U.S.A. FORM NO. 8131-1

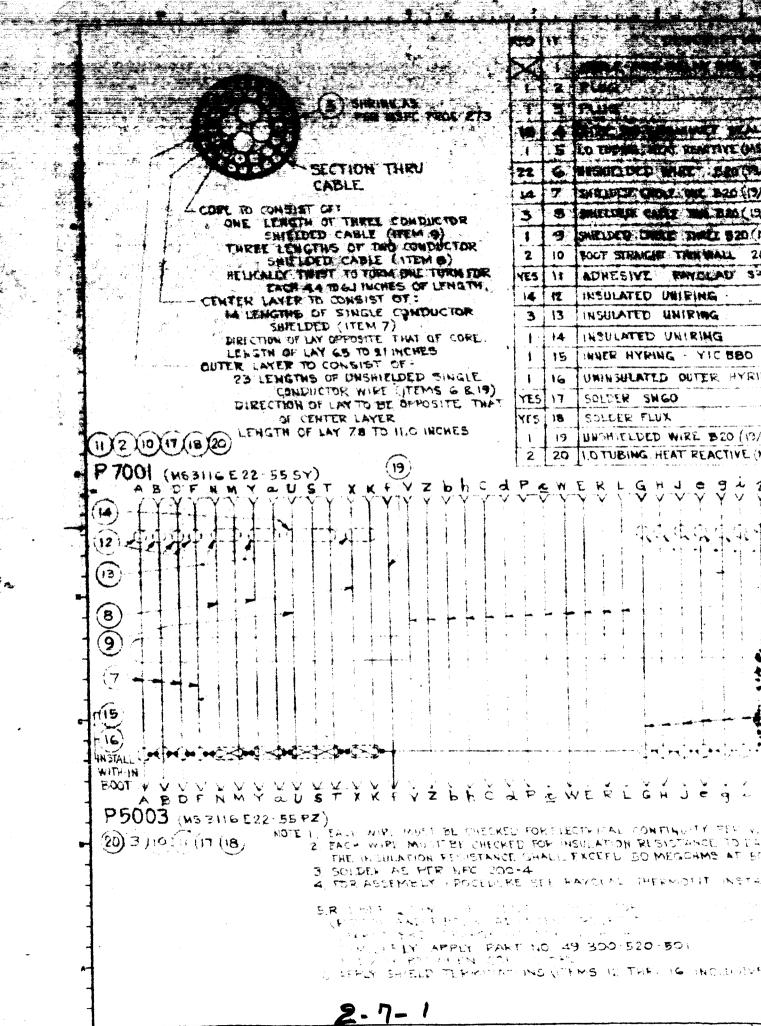


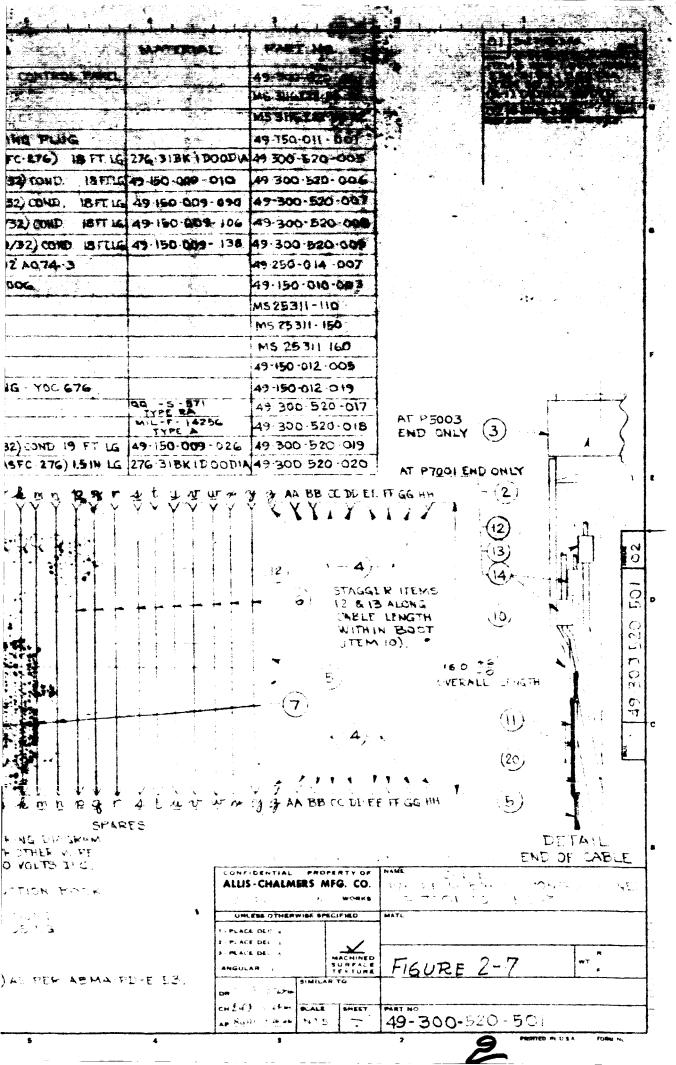


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2 EACH WIRE MUST BE CHECKED FOR INSULATION RESISTANCE TO EACH
THE INSULATION RESISTANCE SHALL EXCEED SO MEGOHMS AT
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BRUBBER STAMP OR STENCIL CONNECTOR IDENTIFICATION NUMBERS (F RESPECTIVE CONNECTORS USING CHARACTERS APPROXIMATELY .) SIMILARLY APPLY "PART NO. 49-300-306-301 MIDWAY BETWEEN G APPLY SHIELD TERMINATIONS (ITEMS 12 THRU 16 INCLUSIVE) AS







provides additional information on the recommended test setup for the gases, liquid coolant, and the product water.

<u>CAUTION</u>: Care should be exercized in making all connections to prevent damage to electrical connectors and to insure leak tight tube connections. Refer to Paragraph 2.2 <u>Initial Installation Checkout before making any external interface connections</u>.

- C. A data acquisition system and direct readout equipment, which must also provide the excitation voltage for the five (5) Allis-Chalmers transducers to be monitored. A listing of the recommended functions and the method of monitoring or recording is contained in Figure 2-8.
- D. Temperature recording equipment will be required for fuel cell temperatures. Allis-Chalmers will furnish mating connectors for the fuel cell module instrumentation, but not the cable. All thermocouple connections will be made up for iron constantan couples. No reference junction compensation circuits are furnished.
- E. The 400-cycle three-phase power for the fuel cell coolant fans rated to supply at least 150 watts at 200 volts.
- F. The customer will furnish the electrical load bank for the fuel cell output capability testing and the load disconnect contactor.

RECOMMENDED MONITOR FUNCTIONS FOR SYSTEM #5R

		Digitec	Panel Meter	VIV Recorder	Data Acquis.	Other
1.	Total fuel cell voltage	-	v	•	•	
2.	Total fuel cell current Both on Panel Control		x x	x x	x	
3.	Stack temperature (TC-8 and TC-9)		^	x	x x	
4.	Cavity pressure	x		x	x	
5.	Individual cell volts	x		A	x	
**6.	Fan current	Α	x		x	
7.	Heater current (28 vdc, 1600 watts)		x		x	
8.	H ₂ inlet pressure	x			x	
9.	O ₂ inlet pressure	x			x	
10.	Canister pressure	x			x	
11.	-5. 0 vdc				x	
12.	+11.2 vdc				x	
** 1 3.	System "ON" lapse time		x			
4.	Load "ON" lapse time		x			
**15.	WRS heating tape temperature		x		x	
16.	Stack thermocouples - inside (7 additional)				x	
17.	Fan No. 1 RPM	x			×	
18.	Fan No. 2 RPM	×			×	
**19.	Fan Voltage				x	
20.	Stack liquid coolant differential pressure				x	
*21.	Stack liquid coolant outlet temperature				x	x
*22.	Liquid coolant inlet temperature					
**23.	Inlet liquid coolant flow					
* *24 .	Liquid coolant-inlet pressure				x	
**25.	Liquid coolant-outlet pressure				x	
* *26.	Helium inlet pressure		• •		x	
×× 27.	H ₂ supply pressure		x		x	
	O ₂ supply pressure		x		×	
	Barometric pressure				x	

^{*} Function has changes of short duration requiring continuous recording if detailed information is required.

^{**} Sensors to be provided by NASA.

2.1.5 Supplementary Installation Information

Figure 2-9 (Connector Interface function description) contains additional interface information to aid in the assembly of the test setup.

2.2 INITIAL INSTALLATION CHECKOUT

2.2.1 Electrical Testing

The external interface connections should be verified as per Figure 1-2A, 1-2B, and 1-2C (Drawing No. 49-500-125-404) and Figure 2-2A (Drawing No. 49-400-260-405), NASA's interface should be checked prior to the initial application of any power or reactants.

Instrumentation calibration data for use during checkout and operating can also be found in Figure 2-9.

2.2.2 Leak Test

Prior to the initial operation of the fuel cell, the reactant gas system, the water removal cavity, and the canister enclosure must be subjected to a leak test. The following is the procedure for performing this test, but it should not be performed initially without a representative from Allis-Chalmers present. Figure 2-10 is a suggested schematic only.

J5001-NASA Control Panel

- A + 28 vdc input from fuel cell
- B 28 vdc input from fuel cell and main ground

J5002-NASA Control Panel

- A + 28 vdc input from auxiliary supply
- B 28 vdc input from auxiliary supply and main ground.

J5006-NASA Control Panel

- A Logic signal ground output
- D +11.2 vdc logic control voltage output for monitor only
- F -5.6 vdc logic control voltage output for monitor only
- V + 28 vdc valve power output for monitor only
- K + 28 vdc output to main heater control for 1,600 watt heater
- G 28 vdc ground output to main heater control for 1,600 watt heater
- S + 28 vdc output to trip main circuit breaker
- U + 28 vdc output to close main circuit breaker
- H 28 vdc ground output to main circuit breaker

Optional Monitor Signals

J5006-B Amp-hour readout - NOTE: This signal is displayed on panel (Amp-Hour Counter)

J3003 - 1,600 watt heater

- E + 28 vdc 29 amp heater power for first 800-watt heater
- G 28 vdc ground heater power for first 800-watt heater
- C 800-watt heater thermostat N.O. for first
- H 800-watt heater thermostat N.O. 800-watt heater
- M Shield for Pins C and H, isolated from stack
- J + 28 vdc 29 amp heater power for second 800-watt heater
- K -28 vdc ground heater power for second 800-watt heater
- A 800-watt heater thermostat N.O. for second
- B 800-watt heater thermostat N.O. 800-watt heater
- L Shield for Pins A and B, isolated from stack

J1000- Fuel Cell Fans and RPM

- E Fan reluctance pickup "AC" side, output signal 150 millivolts peak-to peak at approximately 1300 cps representing 20,000
- F RPM to be fed into AC to DC converter for instrumentation readout.
- G Shield for Pin E and F.
- J Fan reluctance pickup "BC" side, output signal 150 millivolts peak-to peak at approximately 1300 cps representing 20,000
- H RPM to be fed into AC to DC converter for instrumentation readout.
- T Shield for Pin J and H
- A Phase "A" Fan power input for A-C Side, 200 Vac,
- B Phase "B" 400 cps, 3-phase at approximately
- C Phase "C" 0.15 amp. per phase
- D Shield for Pins A, B, and C carried through to motor, isolated from case ground.
- K Phase "A" Fan power input for B-D side, 200 Vac.
- L Phase "B" 400 cps, 3-phase at approximately
- M Phase "C" 0.15 amp. per phase
- N Shield for Pins K, L, and M carried through to motor, isolated from case ground.

CELL VOLTAGES - SYSTEM # 5R Connectors J1002 and J1003 On The Fuel Cell

Cell No.	Plus Pin	Minus Pin
1	Ј1003Ь	J 100 2b
2	Ј 1002Ь	J1002a
3	J1002a	J1003a
4	J1003a	J1003Z
5	J1003Z	J1002Z
6	J 1002 Z	J1002Y
7	J1002Y	J 1003Y
8	J1003Y	J1003X
9	J1003X	J1002X
10	J1002X	J1002W
11	J1002 W	J1003W
12	J 1003W	J1003V
13	J1003V	J1002V
14	J1002V	J1002U
6 5	J1002U	J1003U
16	J 1002U	J1003T
17	J1003T	J1002 T
18	J 1002 T	J1002S
19	J1002S	J1003S
20	J1003S	J1003R
21	J1003R	J1002R
22	J1002R	J1002P
23	J1002P	J1003P
24	J1003P	J1003N
25	J1003N	J1002N
26	J1002 N	J1002M
27	J1002 M	J1003M
28	J1003 M	J1003L
29	J1003L	J1002L
30	J1002L	J1002K
31	J1002K	J1003K
32	J1003K	J1003J
33	J1003 J	J1002J
Spare Pins		

J1002 - A,B,C,D,E,F,G,H J1003 - A,B,C,D,E,F,G,H

Pin c left open for cable shield tie point Pin c left open for cable shield tie point

Transducer Calibration Data

Note: All Transducers - 5000 - 100 ohms element-max current 10 ma

J3001 Fuel Cell Pressure Transducer

O2 Inlet absolute pressure transducer (pin i transducer ground) i + Excitation voltage h - Excitation Voltage and - signal output ſ + Signal output, 0-50 psia - 1% g Sensitivity 0.02 volt/psia/volt excitation H₂ Inlet absolute pressure transducer (pin a transducer ground) \mathbf{a} Z+ Excitation voltage X - Excitation voltage and - signal output + Signal output, 0-50 psia ± 1%. Y Sensitivity 0.02 volt/psia/volt excitation Canister pressure transducer (pine transducer ground) G d + Excitation voltage - Excitation voltage and - signal output b + Signal output, 0-50 psia - 1% C Sensitivity 0.02 volt/psia/volt excitation Liquid coolant differential pressure transducer (pin J transducer ground) J H + Excitation voltage F - Excitation voltage and - signal output G + Signal output, -10 to + 10 psid -1.25%Sensitivity 0.05 volt/psid/volt excitation Water cavity readout pressure transducer (pinW transducer ground) W V + Excitation voltage T - Excitation voltage and - signal output U + Signal output $0-\overline{2}5$ psia -1%. Sensitivity 0.04 volt/psia/volt excitation LIQUID COOLANT VALVE SUPERVISORY CONTACTS Monitor signal - coolant valve close В C Input signal to coolant valve connections D Monitor signal - coolant valve open

OXYGEN PURGE VALVE SUPERVISORY CONTACTS

j k m	Monitor Signal - O ₂ Purge Valve Close Input Signal to O ₂ Purge Valve Connections Monitor Signal - O ₂ Purge Valve Open
	HYDROGEN PURGE VALVE SUPERVISORY CONTACTS
n p q	Monitor Signal - H, Purge Valve Close Input Signal to H, Purge Valve Connections Monitor Signal - H, Purge Valve Open
	REACTANT INLET VALVE SUPERVISORY CONTACTS
k L m	Monitor Signal - Reactant inlet valve close Input signal to reactant inlet valve connection Monitor Signal - Reactant inlet valve open

J1005 FUEL CELL THERMOCOUPLE - INSIDE OF STACK

Pin	Polarity	Thermocouple No.	Location
A	Plus	1	In H ₂ O Plate#45-Corner A (Cell #11)
В	Minus		
С	Plus	2	In H ₂ O Plate#5 - Corner C(Cell #4)
D	Minus		2
E	Plus	3	In H ₂ O Plate #129-Corner D (Cell#33)
F	Minus		-
G	Plus	4	Under Heat Exchanger
Н	Minus		1
J	Plus	5	Fan Outlet Return A-C Side
K	Minus		
L	Plus	6	Fan Outlet A-C Side
M	Minus		
N	Plus	7	Fan Outlet B-D Side
\mathbf{P}	Minus		
R	Plus	8	In Transister holder between O ₂ Plate
S	Minus		#75 and H ₂ Plate #72-Corner A ² (cell 19)
${f T}$	Plus	9	In Transistor holder between O2 Plate
U	Minus		#67, and H ₂ Plate#64-Corner D(cell 17)

Note: Plus is iron - Yellow

Minus is constantan - Red

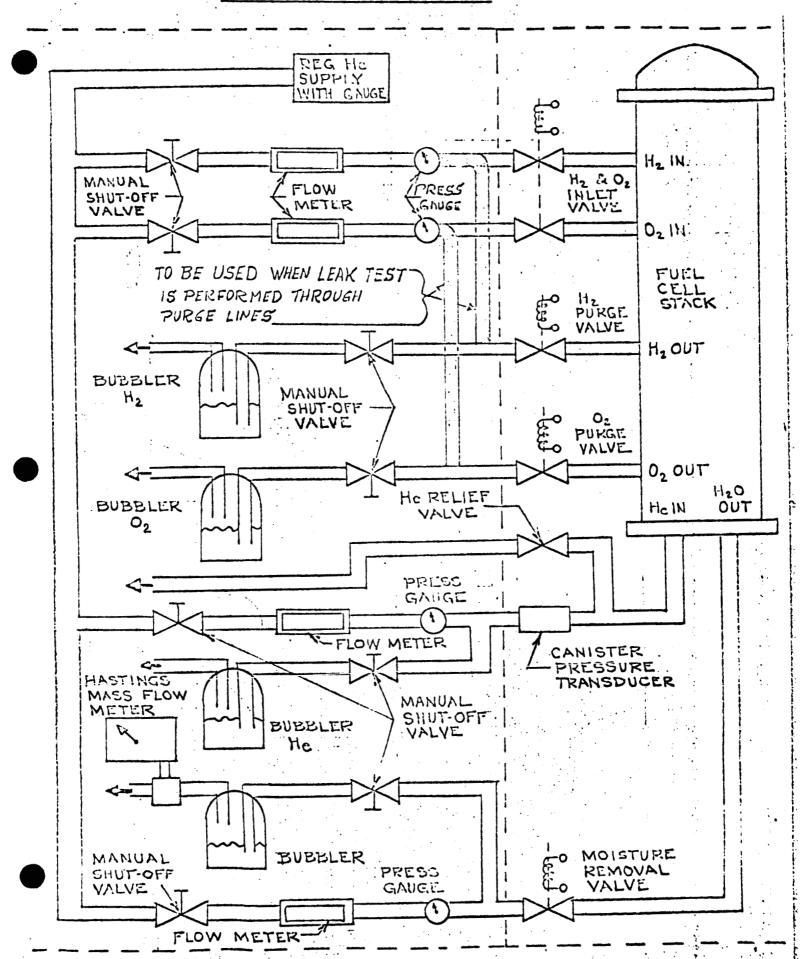


Figure 2-10

A regulated helium gas supply should be connected to each of the following lines on the fuel cell module.

- (1) Hydrogen gas inlet or hydrogen purge line
- (2) Oxygen gas inlet or oxygen purge line
- (3) Helium gas inlet
- (4) Moisture removal line (vapor vent)

The water vapor outlet from the fuel cell stack should be connected through a manual shut-off valve to a gas bubbler and a Hastings Mass Flowmeter for visual observation. The helium supply line to each of the above points should contain a manual shut-off valve and a pressure gauge downstream of the shut-off valve. A flow meter in each line is desirable but not mandatory. The hydrogen purge outlet and oxygen purge outlet should also discharge to the atmosphere through manual shut-off valves.

The detailed leak test procedure is as follows:

Cavity External Leak Check

- (1) Bleed the helium pressure within the fuel cell canister to0 psig from the helium fill line.
- (2) Fill the reactant cavities with helium through the hydrogen and oxygen inlet lines or through the hydrogen and oxygen purge lines to 20 psig, and then depressurize to zero psig. Repeat.
 - CAUTION The pressure should be increased or reduced gradually to insure that the maximum pressure difference between the hydrogen and oxygen pressure gauges is less than 2 psi.

- (3) Close the purge valves (only when reactant cavities are filled through oxygen and hydrogen inlet valves), open the moisture removal cavity valve and the vapor vent.
- (4) Apply helium pressure simultaneously to all three cavities until a pressure of 20 psig is reached, and allow to stand for ten (10) minutes. Observe the Caution note from Step 2.
- (5) Shut off the supply valves and record the three cavity pressures after allowing to stand for 15 minutes. A pressure drop is indicative of a leak into the canister interior or valve leakage. The purge valve leakage may be checked by connecting the purge outlet lines to a gas bubbler. Leakage into the canister may also be checked by putting a bubbler on the canister helium fill line.

Cavity Cross Leak Check

- (6) Open the helium supply valves and raise all cavity pressure back to an equalized pressure of approximately 20 psig and then close the hydrogen inlet or hydrogen purge valve and moisture removal valve.
- (7) Continue to raise the pressure on the oxygen cavity, through the oxygen inlet line or oxygen purge line until a pressure of 22 psig is reached. Close the manual oxygen inlet valve or oxygen purge valve. Allow to stand for 15 minutes and record the reactant cavity pressures. A simultaneous drop in the oxygen cavity pressure and rise in the hydrogen cavity pressure is indicative of a cross leak.

- (8) Open the moisture removal cavity valve and bleed the pressure gradually to zero (0) psig. Open the hydrogen and oxygen inlet valves and gradually pressurize both reactant gas cavities to thirty (30) psi differential across the water removal matrices. Leave the inlet or purge valves open. Allow to stand for 15 minutes and record the bubbles per minute observed in the vacuum vent line gas bubbler and record the Hastings Mass Flowmeter reading.
- (9) Gradually bleed down all helium pressure to zero (0) psig.

Canister Leak Check

- (10) Pressurize the fuel cell canister to 40 psi differential across the canister wall and open the purge lines and vacuum vent line from the vent graduate, to bubblers for visual observation. Disconnect the helium supply from the helium fill line thereby isolating the canister. Record canister pressure every half hour for twenty-four (24) hours along with room temperature. If at all possible, the room temperature should be held constant throughout the test.
- (11) Any observable pressure drops during the tests detailed in Steps 1 through 10 should be reported immediately to the Allis- Chalmers designated representative or site representative. Any flow rate reading in excess of 25 cc/hour observed during the leak test outlined in Step 8 should be reported immediately to Allis-Chalmers. If the pressure drop during the fuel cell canister leak test as detailed in Step 10 exceeds one (1) psi in the twenty-four (24) hour test period, notify Allis- Chalmers.

2.2.3 Heating Tape

To prevent the product water vapor from condensing in the water removal line, the line must be heated from the moisture removal valve at the bottom of the fuel cell module to the water recovery condenser. A section of heating tape is provided for this purpose. The tape is applied by removing its backing and sticking it directly to the water removal manifold and tubing. Cut the tape to the desired length and attach the input leads as per Figure 1-2A (Drawing No. 49-500-125-404). The A-C power input to the input leads on breaking tone is provided from a Variac (See Figure 3-4).

Upon initial startup, adjust the temperature of the water removal line to 195⁺₋ 10°F as follows:

- a. Attach a thermocouple to the tubing to read tubing temperature.
- b. Turn off 110 vac heater power "ON" after first assuring the Variac is set for minimum voltage.
- c. Gradually, raise the heating tape voltage by turning the Variac clockwise until the desired steady-state tubing temperature is reached.

SECTION III

INTEGRATED SYSTEM OPERATION

3.1 GENERAL

This portion of the instruction manual covers the various operational modes of the complete fuel cell assembly, and includes the expected readings of all essential instrumentation. The description of the subsystems, and the thermocouple instrumentation are presented in Section IV of this manual.

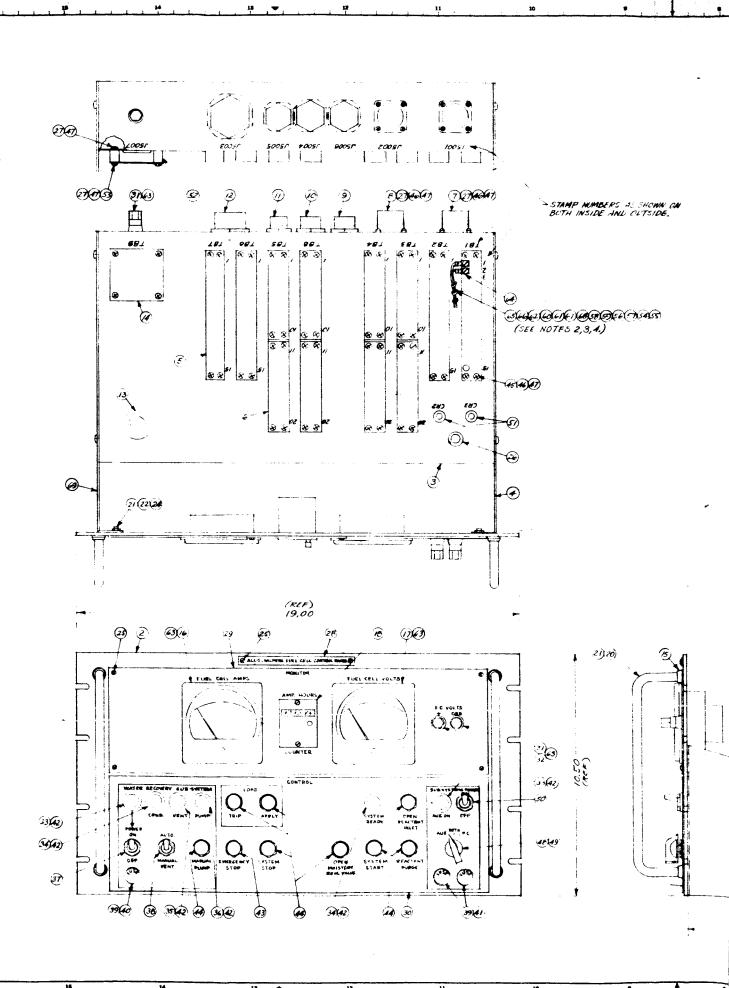
3.2 PRE-STARTUP CONDITIONING OF THE SYSTEM (See A-C control panel Figure 3-1 (49-400-317-401), Figure 3-2 (49-200-549-501), Figure 3-3 (49-500-167-401) and NASA Control Panel Figure 3-4(49-400-349-402).

3.2.1 Initial Conditions

Pre-startup conditioning will be initiated with all valves closed, all switches off, and with system supplies as follows:

- Hydrogen—per NASA specifications with minimum purity of 0.9998

 -Regulator closed off,
- Oxygen per NASA specification with minimum purity of 0.99995 —Regulator closed off,
- Helium Commercial Grade
 —Regulator closed off,
- Vacuum— normal vacuum of at least 1.5 psia applied to the moisture removal line.



3-1-1

01 4444 8.88 ROM THEN MAISTURE BEN. WILVE" AND () MICHELLEN AND () 02 5-4-66 NFH REM NOTES: I. FOR WIRING SCHEMATIC, SEE DWG. 49-500-167-401. 2. SOLDER WHERE REQUIRED, PER NEC-200-4. 3. HEAT SHEINK TUBING PER MSFC-PRCC-273. 4. ROUTING, CPIMPING, LACING, ETC PER ELECTRICAL FAEFICATION PROCEDURE MISTO-PROC-286. 5. CHECK FOR CONTINUITY FER SCHEMATIC. 13 USED ON P/L 49-200-549-501 ALLIS-CHALMERS MFG. CO. ALLIS - CHALMERS PESEARCH 3341 * CONTROL PANEL ASSEMBLY PIX UHLESS OTHERWISE SPECIFIES PLACE DEC . 2422 WT . 13.00 (REF) m J#166 DS# CH 2.63.4-8-4 49-400-317-**4**01 49-400-317-401 02

REQ.	TEN	DESCRIPTION	PART NUMBER
X		CONTROL PANEL ASSEMBLY PIX	49-400-317-401
	2	PANEL	49-300-530-001
\	6	CHASSIS BASE	49-400-347-001
\	N	RIGHT HAND BRACKET	49-300-531-001
4	5:	TERMINAL STRIP CINCH-JONES #15-140Y	49-200-549-005
à	2	YO71-01# " " " "	49-200-549-006
		CONNECTOR, BENDIX	MS3102E18-3P
	α	1	MS3102E18-3FX
	0	"	MS3114E14-19SW
	10		MS3114E14-58
			M83114E12-10S
	2		MS3114E22-558Z
	1	CROWNET 62 12 (25 CD. RUBBER	49-200-549-613
	177	+	49-200-611-501
*	15	+-	49-200-549-015
	2	+	49-200-540-016
\	17		49-200-549-017
\	37	1	49-200-549-018

49-500-167-401

19 SCHEMATIC WIRING DIAGEDM

7	20 	HANDLE, PRETISSING ALETO, PARIDICESS	49-266-540-026
01	12	MACHINE SCREW #10-24 x. 38, CROSS-REC, FLAT HD, CRES	MS24693-70
9	22		+01.6x9585W
4	23	MACHINE SCREW #10-24 x . 35 CROSS-REC. PAN HD, CRES	MSS1957-61.
9	24	LOCKWASHER, #10, SPLIT TYPE, CRES	MS35338-B1
Ø	25	<u> </u>	MS51957-2
/	2.6	GROMMET, 38 1.2, 62 O.D, KUBBER	49-200-549-026
91	27	MACHINE SCREW #4-40+,38, CRUSS REC. FAN HD, CRUS	MS51957-15
\	82	NAME PLATE	100-821-001-64
\	52	MONITOR SECTION PANEL	100-825-008-64
\	30	CONTROL " "	49-30-625-005-67
N	3/	EINDING FUST, BLACK, SUPERIOR DF30BC	49.200-549-031
\	32	" " RED " DF3QRC	45-20-540-032
7	33	LENS, RED, SYLVANIA TYPE BOILD	257-845-502-5H
N	核	" GREEM, " " BO112	40-200-540-134
\	33	, ,, ,	49-206-549: 635
\	36	"	# 922-645-002-64
\	25	TOGGLE SWITCH, SPST, CUTLER-HAMMER, 8803, CM. HOWE OFF 49- 240- 545-65	152-695-072-65
/	38	" " " DPDT, " " BBZS, CIRC. CN-NOWE. ON 49-21-549-63	19-22-012-112-64
3	30	FUSEHOLDER, BUSS TYPE HKP	49-200-545-639
/	40	FUSE, STD. TYPE 3AG, 32V, 4AMPLITTELFUSE SEPIES 311000	49 200 640-140
N	41	15 15 15 15 18 18 18 18 18 18 18 18 18 18 18 18 18	49-540-549-041
9	42	HOUSING SLAMP COMPINATION SKIVELA CAIN, ISPOSTEDORS -	49-200-548-142-

		87	FUSH BUTTON SWITCH, MONEUMER	CANENDERY SPST-NO, RED, ARROW-HART 339/61 49-260-549-643	4RT 3391GL	49-260-549-643	F
	Ja	44	+	" 1700 " " " " "	**	40-700-04	1
1	3 8	45	+-	MOTHING SCREW #4-40.x.50 CROSS-KEC, PAN HD, CRES		14551951-11	
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*		40	-	CK OKECITE MILL MED CIPL MAN	HOWE OFF	49-200-549-050	
	/	50		TOGGLE SWITCH UPSI, CLILLER HORINGTON TODE WITCH A	7	130-645-002-64	1
	U	51	SILICON RECTIFIER, TO	51 SKICON RECTIFIER, TEXAS INSTRUMENT TITE THE		49-200-549-052	G
G	A	25	NYLON SPACER, 25 0.D. 1.75 16, #4.40 140.	15 16, #4.40 IND.		WC15795-803	
<u>. </u>	7	ググ	K3 WASHER, FLAT, 1/25 1.0, .250 0.0, CKES	D250 O. U., CKES		Opril out out	
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J .	.***			ARCH	SIMILAR TO	49-200-495-504-302-508	
3	•	1		39-91-4 18-16 OHO 8, PS, 4-16-66	9. SHEET /	10 200 IN 110 COL	
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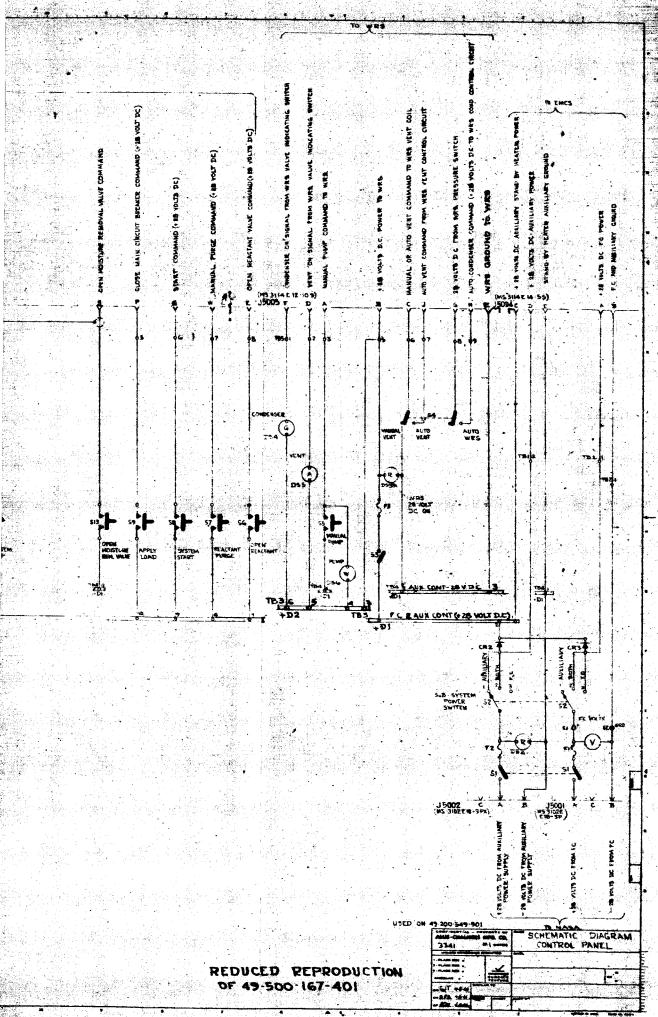
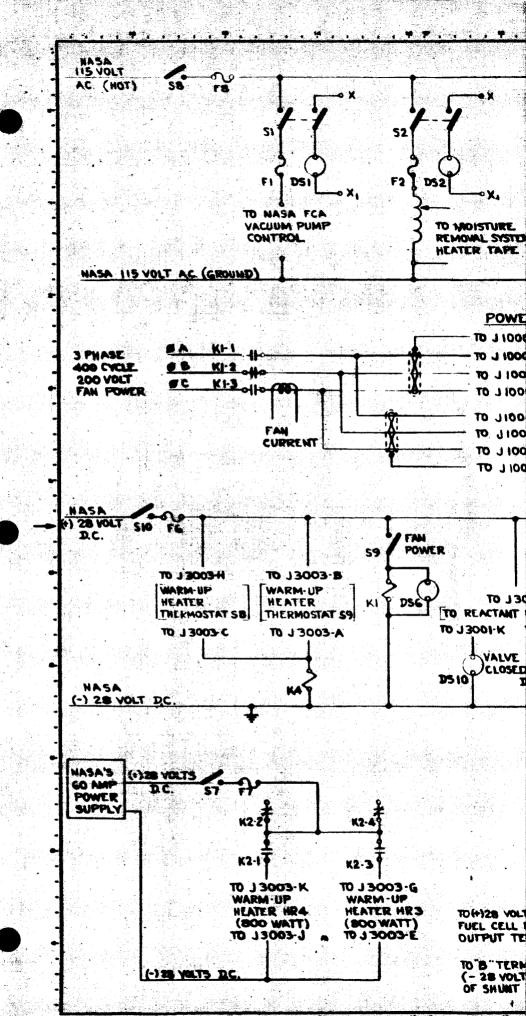
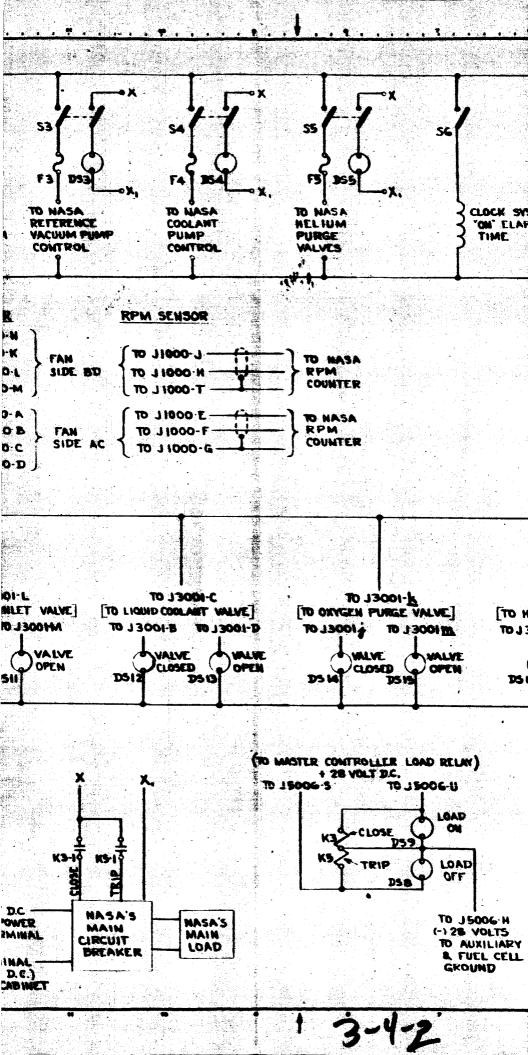
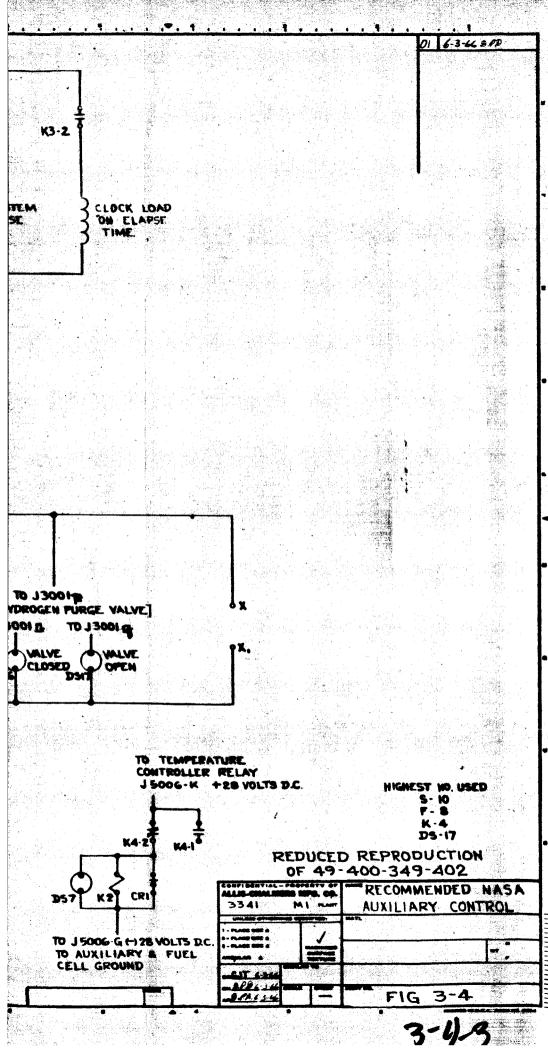


FIGURE 3-3-2



3-4-





Liquid coolant supply available to the canister heat exchanger at a minimum rate of 150 pounds per hour.

110 volt, 60 cps power available at the NASA Test Control Panel

200 volt, 400 cps three-phase power available at the NASA Test Control Panel,

28 vdc auxiliary power available at the NASA Test Control Panel.

3.2.2 Cavity Helium Fill

Fill the three fuel cell cavities (hydrogen, oxygen, and water removal) with helium using the following procedure.

- a. Apply 28 vdc auxiliary power to the EMCS.
- b. Apply power to the helium purge (crossconnect) valves.
- c. Open the moisture removal (cavity) valve.
- d. Open the reactant inlet valve, or open purge valves if helium is supplied through purge lines.
- e. Open the helium supply valves to permit helium flow into the three cavities.
- f. Slowly raise the helium pressure to 5 psig. Allow 5 minutes for stabilization.
- g. Return all switches and valves (Steps b through f) to their original position.

3.2.3 Canister Helium Fill

To evacuate and fill the fuel cell canister with helium to 13 psig, proceed as follows:

a. Open manual valving between the canister and the vacuum header, and evacuate the canister. Monitor the canister pressure.

- When the canister is complely evacuated, close the manual valve b. between the canister and the vacuum header.
- Raise the helium supply pressure to 30 psig. c.
- Crack open the manual valving between the helium supply and the d. canister, and gradually fill the canister to a pressure of approximately 13 psig (28 psia on the pressure transducer output).
- Repeat Steps a through d, then close the manual helium supply valve e. to the canister.

3.2.4 Coolant Fans

Start the coolant fans, and check the fan voltage and current to determine if they are within acceptable limits.

3.2.5 Liquid Coolant System

Start liquid coolant system, and check the coolant pressure and flow to insure it is within acceptable limits.

3.2.6 Water Removal Heating Tape

Apply power to the WRS heating tape and check to insure the tubing rises to the proper temperature range.

3.3 SYSTEM STARTUP (See A-C control panel Figure 3-1 (49-400-317-401), Figure 3-2 (49-200-549-501), Figure 3-3 (49-500-167-401) and NASA Control Panel Figure 3-4 (49-400-349-402). Initial Conditions

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After the conditions of the pre-startup are met, a normal startup will be initiated with the system supplies set as follows:

Hydrogen — Set the house regulator to deliver an outlet pressure of between 200 and 400 psia. The fuel cell hydrogen regulator is set to deliver a pressure output of approximately 37 psia over the full flow range (0.04 to 0.75 pounds per hour).

Oxygen — Set the house regulator to deliver a pressure of between 200 and 400 psia. The fuel cell oxygen regulator is set to deliver a pressure output of approximately 37 psia over the full flow range (0.32 to 6.0 pounds per hour).

Helium — Set the house regulator to deliver pressure of 40 - 2 psia, for the WRS pump.

Liquid Coolant — applied to the fuel cell as specified in Paragraph 3.2.1.

Vacuum — Applied as indicated in Paragraph 3.2.1

Auxiliary Power — Applied to EMCS

Fan Power -- ON

WRS Heater Tape Power - ON

3. 3. 2 Startup Sequence

- a. Vent the moisture removal cavity into the vacuum system. Check the cavity pressure transducer to determine if the cavity has vented.
- b. Press the System Start switch. This applies power to stand-by heaters (50-watt each 100-watt total) and turns ON the warm-up heaters (800 watt each 1600 watt total) providing the 1600 watt switch is ON.

c. Monitor the fuel cell stack warm-up until the operating temperature (185°F) is reached. The heater is controlled by a stack thermister to automatically cut-out at 185°F. The individual heaters are protected by over-temperature thermostats on the heater surfaces set for 250°F.

Note: For initial startup, allow the system to stabilize and monitor the performance of the temperature controller for one hour.

- d. After fuel cell has reached its operating temperature, the "System Ready Light" will come ON, and the reactant inlet valve can be opened to allow hydrogen and oxygen enter the reactant cavities.
 - Note: During initial checkouts and until sufficient testing has been conducted to demonstrate system operational response and stability during startup, it would be desirable to gradually buildup the reactant pressures in the hydrogen and oxygen cavities rather than applying full cavity pressures instantaneously. This may be accomplished by manually controlling pressure buildup using the reactant supply regulators.
 - 1. With both the hydrogen and oxygen supply regulators shutoff, press the Open Reactant button and check that the reactant inlet valve is open (light indication).
 - 2. Slowly bring up the hydrogen and oxygen supply pressures, simultaneously using the supply regulators. Maintain hydrogen and oxygen pressures with 2 psi of each other during this procedure.
 - 3. When rated cell pressure (37 psia) is reached, the fuel cell regulators will maintain this pressure and the supply pressures can be set as indicated in Paragraph 3.3.1 "Initial Conditions"
- e. Check the hydrogen and oxygen pressure transducers. Both transducers should indicate 37 1 psia.

- f. Check that the water removal pipe is hot, approximately 190°F.
- g. Purge the reactant cavities three successive times to clean out the helium or any other inerts. This is accomplished by manually closing the reactant inlet supply valves feeding the reactant inlet valve (since reactant inlet valve cannot be closed manually after being open), then opening the hydrogen and oxygen purge valves.

 Then refill the reactant cavities. Repeat the purge cycle until a total of three purges have been accomplished. During these operations, be sure to follow the procedure in the note under Step d, on page 3-5.
- h. Check the individual cell voltages. Should any cell voltage be less than 1.0 volt, two additional manual purges are permitted to attempt bringing up the individual cell voltage.
- i. Monitor the Total Fuel Cell Voltage. The total open circuit voltage should read 35 volts, or more.
- j. Check the canister pressure to insure it is 40 2 psia. If it is not, fill to the required pressure.
- k. Check to insure that the WRS manual by-pass switch (Manual Vent-Auto) is in the "AUTO" position unless open loop tests are planned.

3.3.3 Switching Auxiliary Power To The Fuel Cell Output

After the fuel cell is warmed up to its operating temperature, the auxiliary power may be switched from external power to fuel cell power, or to Fuel Cell and Auxiliary power (both) in which case the EMCS will "Automatically Select" the source with the higher voltage.

(See A-C control panel Figure 3-1 (49-400-317-401),

OPERATION UNDER LOAD Figure 3-2 (49-200-549-501), Figure 3-3

(49-500-167-401) and NASA Control Panel Figure 3-4 (49-400-349-402).

3.4.1 Initial Conditions

Initially, the system is at operating temperature with an open circuit voltage of 35 volts or more. Reactant supplies to the fuel cell are regulated to specified values, and all pressures individual cell voltages, and temperatures are normal. The auxiliary dc power may be supplied from the fuel cell or from an external source, as desired, to meet specific test requirements. The RPM sensors must indicate that both coolant fans are running, and the liquid coolant pressure transducers must indicate that coolant is available.

<u>CAUTION</u>: The fuel cell should not be held in the hot, unloaded condition (total load less than 200 watts) for more than three hours at any one time. Refer to Paragraph 3.6.2 if longer standby periods are contemplated.

3.4.2 External Load Circuits

Since the external load circuits are being furnished by MSFC their description does not form a part of this manual. A pilot relay must be provided to control the external load circuitry as the "Load" relay in the EMCS will only handle 1 ampere maximum.

3.4.3 Load Application

To apply load to the fuel cell system, push the "Apply Load" Button. The load "ON" signal will also initiate an automatic cavity purge cycle whenever it is actuated.

3.4.4 Normal Operating Parameters

After each incremental load change, the following operating parameters should be monitored to insure normal operation:

190° - 200°F Module Temperature - 37 $\frac{1}{1}$ 1.0 psia Hydrogen Inlet Pressure - 37 $^{+}$ 1.0 psia Oxygen Inlet Pressure Moisture Removal Cavity Pres. Varies automatically to maintain proper KOH concentration (See Figure 3-5) 40 ⁺ 2 psia Canister Helium Pressure Load Current Not to exceed 75 amperes continuous, and 150 emperes for 30 seconds. Total Fuel Cell Voltage See Figure 3-5 Reactant Gas Purge Frequency Every 128 ampere-hours Duration 6 seconds H₂ 0.69 lb/hr. Flow Rate: O₂ 5.47 lb/hr.

3.4.5 Automatic Operation

The system will now operate automatically under load and during load changes as long as reactant gases are supplied and all critical parameters are under control. The individual cell voltages should be monitored at least every one-half hour. Should any individual cell voltage fall below 0.5 volts, it is recommended that a manual purge cycle of six seconds duration be initiated. If the individual cell voltage does not remain above 0.5 volts under load, a second manual purge cycle may be initiated. However, to avoid drying-out the cell, only two manual purges are recommended. If the cell voltage cannot be brought up by purging, a cell depressurization cycle should be performed as follows:

a. Remove all load from the fuel cell system.

- b. Close the reactant inlet supply valves.
- c. Monitoring the reactant pressure transducers, apply a manual purge until the pressures drop to atmospheric.
- d. Close the purge valves, open the reactant inlet valve and reapply reactants to the fuel cell.
- e. Reapply a load "ON" signal to the EMCS.
 - NOTE: If after depressurization, the cell voltage fails to rise above 0.5 volt under load, shut down the fuel cell system and immediately notify Allis-Chalmers.
- 3.5 LOAD REMOVAL OPERATION (See A-C control panel Figure 3-1 (49-300-317-401), Figure 3-2 (49-200-549-501), Figure 3-3 (49-500-167-401) and NASA Control Panel Figure 3-4 (49-400-349-402) The "Drop" load or "Trip" load function can be initiated at any time during normal operation by pushing the "Trip Load" Button. This will result in the following:
 - a. The external electrical load on the fuel cell system will be dropped.
 - b. The moisture removal valve will close and remain closed until a load "ON" signal or a manual cavity valve signal is applied.

All other fuel cell system controls will remain operable and the external load may be reapplied by providing an "Apply Load" signal to the EMCS.

Auxiliary DC power will continue to be supplied by the fuel cell if the system controls are so set.

As stated in Paragraph 3.4.1, the Load "OFF" condition should not be maintained for longer than 3 hours at any one time.

3.6 <u>SYSTEM SHUTDOWN</u>, <u>STANDBY</u>, <u>AND STORAGE</u> (See A-C control panel Figure 3-1 (49-400-317-401), Figure 3-2 (49-200-549-501), Figure 3-3 49-500-167-401) and NASA Control Panel Figure 3-4 (49-400-349-402).

3.6.1 System Shutdown

To shut down the fuel cell system, provide a system stop signal to the EMCS. The following actions will occur:

- a. The external electrical load on the fuel cell system will be dropped, if the fuel cell is in a load "ON" condition, and Step b Paragraph 3.5 will thereby take place.
- b. The reactant inlet valve will close, and shut off the supply of hydrogen and oxygen to the fuel cell.

CAUTION:

Manually reopen the reactant inlet valve and reestablish the cavity pressures and maintain cavity pressure balance within 2 psi. The system can be held at open circuit for a short period (6 hours) in this manner or the cavities can be filled with helium in the case of prolonged shutdown.

c. The System Stop signal also opens the circuit to the stack heater controller. The warmup and stand-by heaters cannot be energized until the System Start signal is again applied.

3.6.2 System Standby at Operating Temperature

After a System Stop signal has been applied and the actions indicated in Steps a through c above have occurred, it is possible to hold the system at approximately operating temperature by performing the following:

Apply a "Start" signal which will close the heater circuit. The helium circulating fans must continue to operate. The fuel cell module may be held in this condition for a period not to exceed 6 hours. It will be necessary, however, to continuously monitor the fuel cell so that the following conditions are met.

- a. The fuel cell temperature as indicated by thermocouples should not exceed 200°F.
- b. All external auxiliary power must be maintained.
- c. Assure that water removal heater tape is energized and maintaining the water removal piping temperature. (This is to allow immediate operation when desired instead of requiring a warm-up period).

3.6.3 Prolonged Shutdown

For any period exceeding 6 hours, it will be necessary to complete system shutdown, and to flood all the cavities with helium according to the following:

- a. Shut down the helium circulating fans.
- b. Close any manual valves in the hydrogen and oxygen supply lines to the fuel cell module.
- c. Apply a manual purge signal until the hydrogen and oxygen cavities are at atmospheric pressure.
- d. Close the purge valves.
- e. Perform a cavity helium fill by following Steps b through g of Paragraph 3.2.2.
- f. Check the helium pressure in the fuel cell canister; if it is less than 13 psig follow Steps c and d. Paragraph 3.2.3 to bring the pressure back up.
- g. Switch off all power, and pumps which are used in the test setup.

The system is now secure and may be left inoperative for a prolonged period as long as helium pressure is maintained in the cavities and canister. It is recommended that these pressures be monitored once every hour for the first 24 hours and once every 8 hours thereafter. The

helium pressure should be brought back to nominal values when the following minimums are reached:

- a. The canister pressure drops to 8 psig.
- b. The three cavity pressures drop to 3 psig.

3.6.4 System Storage

The fuel cell stack may be stored indefinitely in its shipping container in a protected area with an ambient temperature of 49°F or higher.

All other components may be stored in protected, but unheated, areas, provided adequate steps are taken to prevent condensation on the components.

3.7 ABNORMAL OPERATION AND EMERGENCY SHUTDOWN

Abnormal operation is defined as any operating condition in which one or more of the critical control parameters exceeds its normal control range. The critical control parameters, their normal range and action to be taken if the control band is exceeded, is presented briefly in this section.

3. 7. 1 Stack Temperature

The normal control range is $195^{\circ} + 5^{\circ}$ F as sensed by the thermister located between plates 80 and 83 on the fuel cell stack. A spare thermister is provided in the same block.

a. Over-Temperature — Over-temperature may be detected by monitoring the thermocouples that form part of the test instrumentation. On an over-temperature indication, check for the following:

- 1. loss of liquid coolant,
- 2. loss of helium circulating fans,
- 3. loss of helium from the canister.

The fuel cell should be shut down immediately if a stack temperature of 220°F is reached. Below this temperature, the fuel cell may be operated up to 3 hours while the cause of the over-temperature is being investigated.

b. Under-Temperature — Under-temperature operation is indicated by a gradual deterioration of cell performance under load, but represents no immediate safety or performance problem. It may be caused by overcooling by the liquid coolant system, or under-heating when operating at light loads in cold environments. To determine the cause, the liquid Coolant Valve should be closed. Monitor the stack temperature for effect. If the temperature begins to rise, a fault exists somewhere in the cooling system. If the temperature remains low, the fault is probably in the heaters or heater controls; this should be checked with the fuel cell system shutdown.

3. 7. 2 Total Fuel Cell Voltage

The normal fuel cell voltage will vary with load, as shown in Figure 3-5 and with fuel cell load life. The operator should be alert primarily for voltage changes during operation at constant load. Should the total voltage change 1/2 volt in 2 hours under a constant load condition, a complete survey of the individual cell voltages should be made.

A decreasing total cell voltage under constant load conditions may be caused by several factors such as:

- a. Accumulation of inerts in the cavities,
- b. Decrease in reactant supply.
- c. Improper operation of the water removal subsystem,
- d. Fuel cell stack temperature too high or too low. (See Paragraph 3.7.1)

Upon detection of an abnormal voltage output drop, the external fuel cell load should be removed, and the open circuit voltage on the individual cells should be checked.

- a. Accumulation of Inerts If the voltage change is due to an accumulation of inerts within one or more of the individual cells, the total voltage will usually show a gradual decrease over a period of hours. The operator may perform two manual purge cycles to bring all the cell voltage to a minimum of 1.0 volts open circuit.
- b. Reactant Cavity Pressures The cavity pressure regulators are set to maintain the hydrogen and oxygen cavities at 37 [†] 1 psia over the fuel flow range. Each cavity pressure is monitored by a pressure switch set to close the reactant inlet valve and to drop the main fuel cell load at a pressure of 44.5 [†] 0.5 psia.

Should the reactant inlet valve close during the operation, the load should be removed and the reactant cavity pressures should be checked immediately. If high reactant inlet pressure is indicated as the cause of the inlet valve closure then the cavities should be manually purged until atmospheric pressure is attained.

Close the manual valves in the reactant inlet lines and flood the cavities with helium to 5 psig. Then check the operation of the reactant gas pressure regulators before restarting the system.

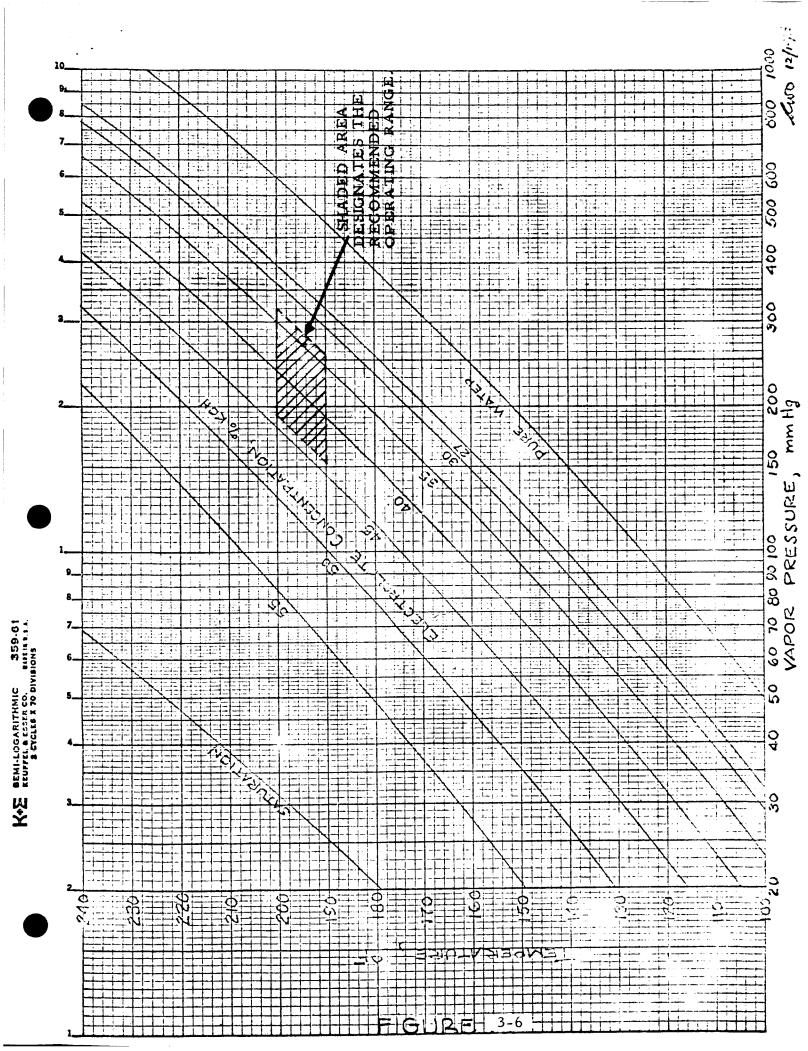
c. Moisture Removal - Moisture removal subsystem malfunctions

may result in a decrease in cell voltage either due to excessive wetting of the cell or excessive cell drying. If the moisture removal valve stays closed, the cell will accumulate too much moisture and the electrolyte will become diluted. To determine if this is the problem, reduce the load to reduce the probability of causing permanent damage and take readings of the cavity pressure and stack temperature. Compare these readings to the allowable operating range as shown on Figure 3-6. Should over wetting prove to be the cause of decrease in cell voltage, the moisture removal valve should be opened and the change in cavity pressure observed. If the malfunction appears to be on the cavity controller, the fuel cell should be shut down and Allis-Chalmers should be notified immediately.

Excessive cell drying can occur if the moisture removal valve is open too long. This condition can be corrected by a period of low load operation with the moisture removal valve closed. Excessive drying can be determined by observing the action of the moisture removal valve, monitoring the cavity pressure, and observing cell voltage for a period of 1 to 2 hours while operating at low load 20 amp). The information obtained should be compared with Figure 3-6. Should cell drying be indicated, the Allis-Chalmers Project Manager or his site representative should be contracted for a detailed corrective procedure.

3.7.3 Canister Pressure

Canister over-pressure protection is provided by a relief valve set to open at a pressure of 45 psia. Canister pressure is monitored by a pressure transducer. Since canister pressure is controlled manually,



it should be monitored periodically and adjusted as necessary to maintain a pressure of 40 ⁺/₋ 1 psia during normal operation.

3.7.4 Loss of Auxiliary Power

If loss of either the 28 vdc or the auxiliary power 200 v, 400-cycle fan power is indicated, the fuel cell should be shut down immediately. Since the reactant inlet valve requires power to close, it is possible to lose auxiliary power and have the reactant inlet valve remain open. Therefore, the first step after loss of auxiliary power is to close the manual valves in the reactant supply lines, and to verify the position of the reactant inlet valve.

3. 7. 5 Emergency Stop

An Emergency Stop signal will perform the following functions:

- a. Close the reactant inlet valve,
- b. Drop the external load,
- c. Interrupt the heater circuit,
- d. Close the moisture removal valve,

The Emergency Stop signal should be used to shut down the fuel cell system any time a malfunction is suspected or a safety problem exists. The Emergency Stop performs essentially the same functions as the System Stop, but it by-passes some of the control system interlocks; its use, therefore, should be limited to emergency conditions. The normal startup procedure should be utilized following an emergency stop.

SECTION IV

SUBSYSTEM DESCRIPTION

4.1 FUEL CELL STACK SUBSYSTEM (FCSS)

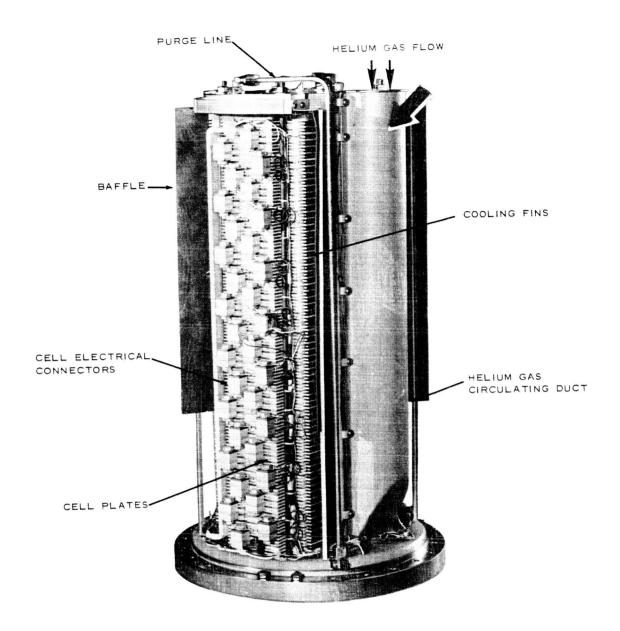
The Fuel Cell Stack Subsystem (FCSS) is the subassembly that converts chemical energy to electrical energy, producing heat and potable water as by-products of the reaction.

4.1.1 Description

The FCSS consists of 33, two-cell parallel connected, sections. The 33 sections are electrically connected in series to produce a nominal 29 vdc output capable of supplying 2,000 watts. Each cell has an effective electrochemical reaction area of 0.20 feet². An asbestos capillary matrix facing the hydrogen electrode provides for removal of the by-product water. The stack subassembly is shown in Figure 4-1. An exploded view of the cell construction is shown in Figure 4-2.

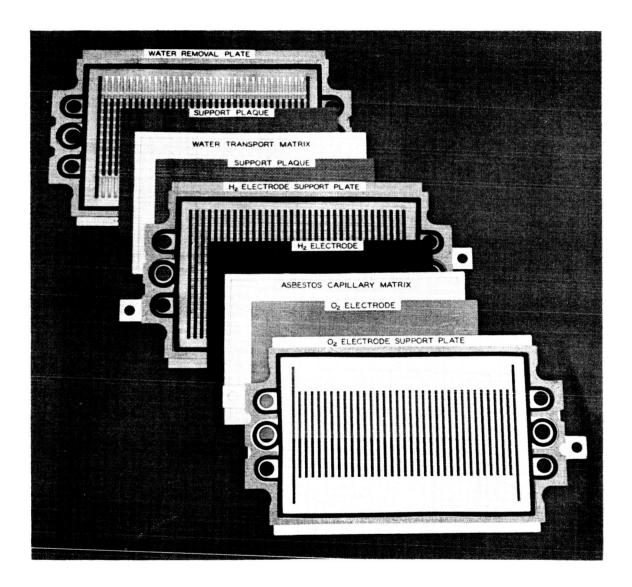
The construction consists of individual cells stacked in a manner that results in common oxygen and water plates for adjacent cells. The electrical connections are provided at both ends of the hydrogen and oxygen plates to minimize the voltage drop due to plate and connector resistance. In addition, electrical connections are silver or gold plated to minimize contact resistance.

The reactants are supplied to the cell plates, and the by-product water is removed, through the main manifolds formed by holes and seals at the end of the plates. The reactants flow from the main manifold holes through electro-discharge machined (EDM) slots in the plates to grooved passages



FUEL CELL STACK. The stack, the power producing element of the system, consists of 33 two-cell sections. Each cell has an effective electro-chemical reaction area of 0.2 square foot. By-product water is removed from the stack in the vapor state using a simple and characteristically stable static moisture removal technique. Plastic ducts (arrow) direct coolant gas over the cell edges for thermal conditioning.

ALLIS-CHALMERS



CELL CONSTRUCTION. The cell consists of two porous electrodes separated by an asbestos capillary matrix, which holds the aqueous potassium hydroxide (KOH) electrolyte. The electrode support plates provide passageways for distributing the reactants to the cell, and serve as current collectors and terminals for the electrodes. Product water is removed via the water transport matrix and the water removal plate as water vapor. When assembled, the plates extend slightly beyond the cell, thus serving as cooling fins for removing waste heat.

on the plate surfaces, providing uniform distribution of the reactants over the electrode surface. By-product water is removed through similar passages and slots.

Heat from the cell reactions is removed by conduction through the metal sections of the cell plates to cooling fins located on two sides of the plates, and with the by-product water vapor.

The cell plates are made of a high thermal conductivity magnesium alloy, and are electroless nickel plated; the oxygen plates have an additional plating of gold.

The seal for containing the reactants and by-product water vapor in the cells is formed by compressing the KOH impregnated asbestos capillary matrix between the plates. A elastomer seal is used to contain the liquid KOH and to contain the reactants and water vapor in the common manifold passageways. An insulating spacer material, 0.065 inch thick, surrounds and contains the elastomer seal. This spacer controls the compression on the cells, moisture removal matrix, and the elastomer seals.

The cells are sandwiched between thermal insulation and end plates and are held in compression by tie rods.

4.2 REACTANT CONTROL AND CONDITIONING SUBSYSTEM (RCCS)

The Reactant Control and Conditioning Subsystem (RCCS) has several functions. It maintains constant hydrogen and oxygen (reactant) pressures within the Fuel Cell Stack Subassembly (FCSS), maintains reactant flow rates as demanded by the FCSS, provides a means of purging the FCSS of inert gas contaminants, and prevents over-pressurization of the FCSS. The reactants are supplied to the RCCS at pressures between

200 and 400 psia, at temperatures between 0 and 150°F, and with purity requirements as noted in Paragraph 3.2.1.

4.2.1 Description

The RCCS consists of three solenoid valves: two pressure regulators, two absolute pressure switches, two absolute pressure transducers, the reactant supplements are functionally arranged as indicated schematically in Figure 4-3. The inlet solenoid valve isolates the Fuel Cell Stack from the reactant supply during non-operation. The pressure regulators maintain constant reactant pressures within the FCSS with a tolerance of $\frac{1}{2}$ l psi at a set pressure of 37.0 psia. The absolute pressure switches prevent damaging pressure extremes within the FCSS in order to maintain reactant purity within the cell. The pressure transducers monitor hydrogen and oxygen pressures to the FCSS The Inlet solenoid valve is equipped with supervisory contacts from which valve position can be monitored. The reactant pre-heaters are used to bring both the oxygen and hydrogen up to operating temperature.

4.3 THERMAL CONTROL AND CONDITIONING SUBSYSTEM (TCCS)

The TCCS is designed to perform the following function:

- a. Bring the fuel cell from 0°F up to 185°F within one hour,
- b. Maintain fuel cell operating temperatures at 195 5°F throughout the operating period,
- c. Monitor the canister pressure and provide canister over pressure protection.

4.3.1 Description

A schematic representation of the TCCS is shown in Figure 4-4, and Figure 4-5. Functions of the major TCCS components are as follows:

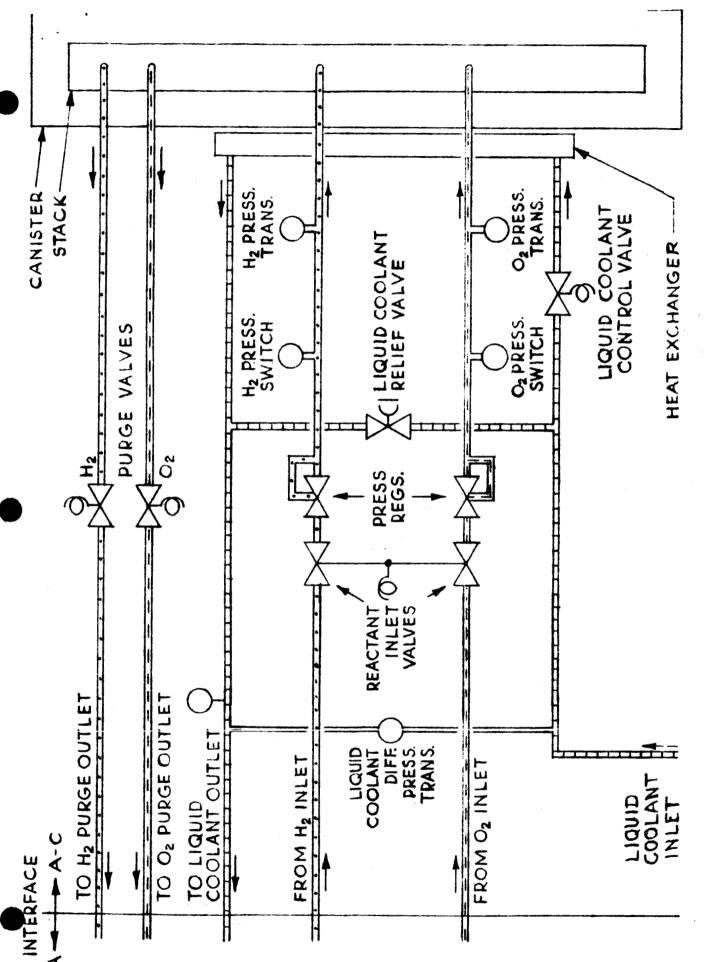


FIG. 4-3 REACTANT CONDITIONING CONTROL SUBSYSTEM (RCCS)

THERMAL CONDITIONING AND CONTROL SUBSYSTEM (TCCS)

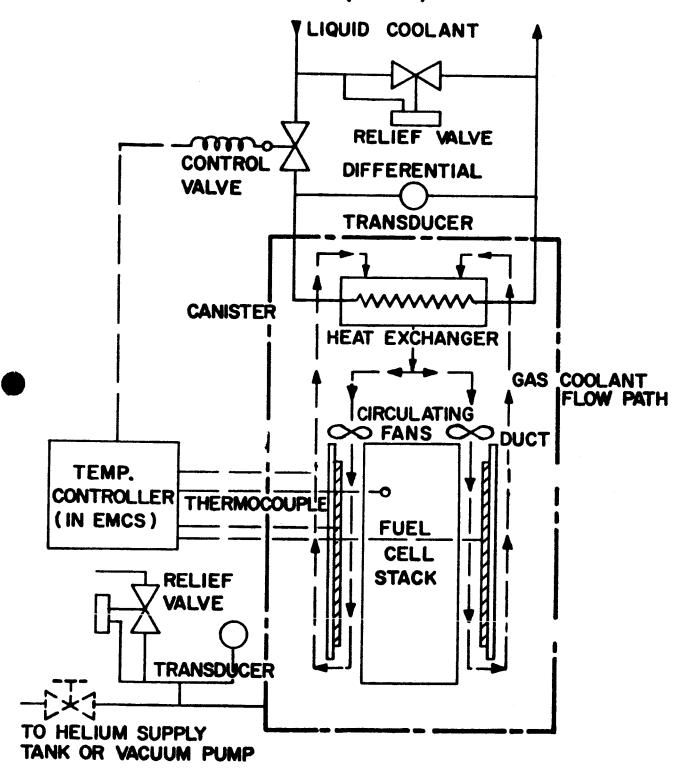
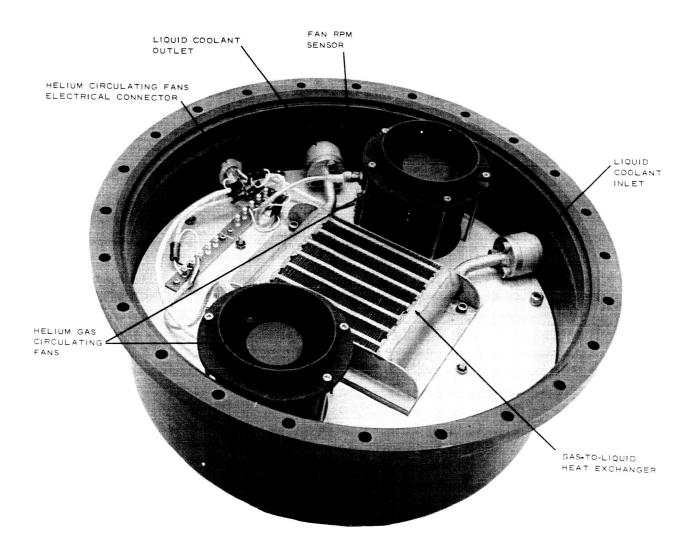


FIGURE 4-4

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THERMAL CONTROL AND CONDITIONING. Circulating fans and a gas-to-liquid heat exchanger, mounted in the canister dome, provide thermal conditioning for the stack. The fans circulate helium gas through distribution ducts, over protruding cell fins, and then through the heat exchanger. Stack temperature is maintained by controlling the flow of liquid coolant through the heat exchanger.

- The warm-up heaters (two 800-watt heaters controlled Warmup a. by the EMCS, powered by NASA) and the stand-by heaters (two 50-watt heaters controlled by the EMCS, powered by the EMCS) heat the helium gas in the canister, and the helium gas is circulated around the FCSS by the fans. This operation transfers thermal energy from the warm-up heaters and stand-by heaters to the FCSS and brings it up to operating temperature. A thermostat senses stand-by heater surface temperature and controls the power input to these heaters, through a solid state switch, such that the surface temperature of the stand-by heaters never exceeds 250°F. The temperature controller senses FCSS temperature when that temperature reaches 185°F, power to the warm-up heaters stand-by heaters is shut off. NOTE: Both type heaters are parallel controlled by the EMCS. However, the 800-watt heater surface temperature can be controlled by NASA through the 800-watt thermostats.
- b. Operating After the FCSS reaches a temperature of 195°F, the TCCS must remove the excess heat generated by fuel cell operation. To accomplish this, the temperature controller senses FCSS temperature through a thermistor and controls the flow of liquid coolant through the heat exchanger, shown in Figure 4-4 by opening or closing the liquid coolant control valve. The liquid coolant control valve opens when FCSS temperature is maintained at 195⁺/₅ 5°F. The helium gas in the canister is circulated around the FCSS and through the heat exchanger by continuous operating fans. The helium gas picks up heat from the FCSS and transfers it to the liquid coolant in the heat exchanger. The liquid coolant, in turn, transports the heat out of the canister to the liquid coolant sink where it is dissipated.

If the level of fuel cell operation is such that FCSS temperature drops below 185°F, the TCCS will go into the warm-up operation to maintain operating temperature. If one desires, the 800-watt heaters can be shut off and additional heating will be accomplished by the 50-watt heaters.

c. <u>Canister Pressurization</u>— The fuel cell canister is evacuated and filled with helium gas to a pressure of 40 ⁺ 2 psia. The operation capacity of the TCCS is dependent upon the characteristics of this helium gas, which is used as a secondary coolant in the TCCS.

Therefore, a method is provided for maintaining canister pressurization as shown in Figures 4-4 and 4-5. A relief valve provides overpressure protection and a pressure transducer provides a method of monitoring. A manually operated valve, located on the opposite side of the system interface, is used for evacuation and fill.

4.4 MOISTURE REMOVAL SUBSYSTEM (MRS)

The Moisture Removal Subsystem (MRS) maintains water removal cavity pressure (utilized in the Static Moisture Removal Concept) equivalent to the water vapor pressure exerted by the most concentrated KOH solution desired in the FCSS water cavity. The regulator opens the valve and vents water vapor from the fuel cell if the cavity pressure exceeds this value.

4.4.1 Description

The design uses a solenoid operated water cavity valve actuated by an electronic temperature compensated controller that receives its signal from a pressure transducer. A schematic diagram of the subsystem is shown in Figure 4-6.

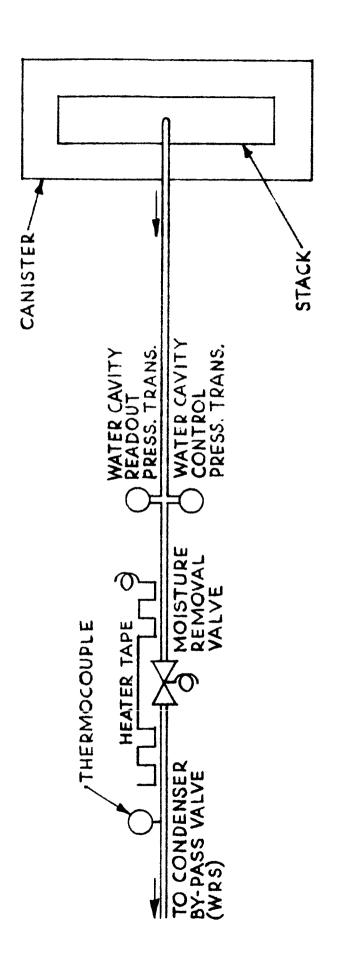


FIG.4-6 MOISTURE REMOVAL SUBSYSTEM (MRS)

4.5 ELECTRICAL MONITORING AND CONTROL SUBSYSTEM (EMCS)

The EMCS consists of a power supply, a temperature controller, a purge controller, a moisture removal controller, and a master controller. These controllers are built-up on a number of printed circuit boards cards, and all are mounted in a single control box. The circuits for these various controllers have been designed to use static control throughout, with the exception of the output devices which are miniature-type latching relays. This arrangement permits isolation of the valve control solenoids from their electronic circuits. A brief functional description of each of the controllers follows in the succeeding paragraphs.

4.5.1 Control Power Supply —

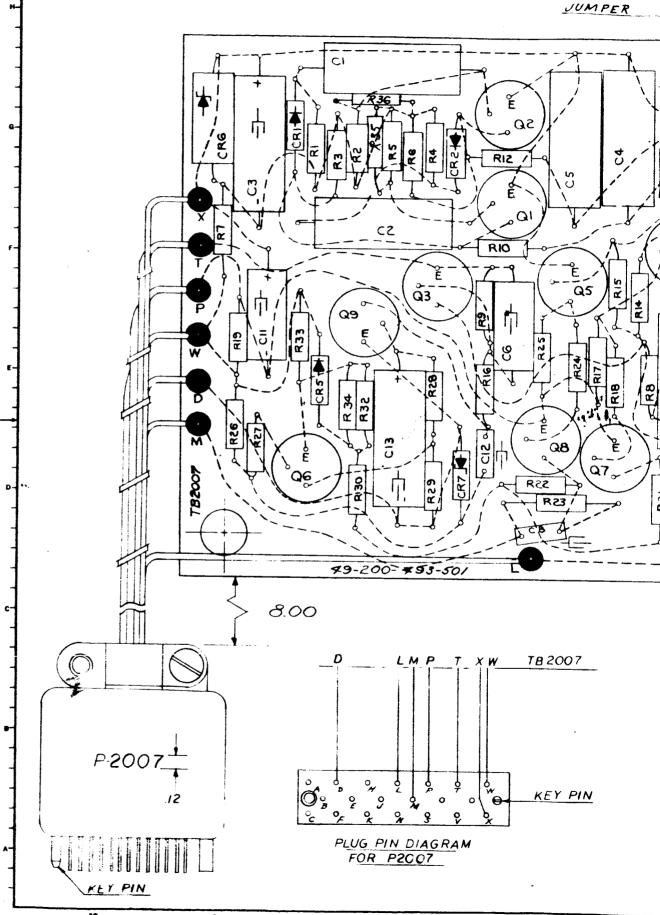
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Figure 4-7 (Drawing No. 49-200-493-501),
Figure 4-8 (Drawing No. 49-300-542-401),
Figure 4-9 (Drawing No. 49-300-496-401),
Figure 4-10 (Drawing No. 49-200-492-501),
Figure 4-11 (Drawing No. 49-200-484-401),
Figure 4-12 (Drawing No. 49-400-300-401),
```

The control power supply provides up to 10 watts of dc. power at the following voltages: $+11.2 \text{ v}^{+} 0.5\%$ and $-5.62 \text{ v}^{+} 0.5\%$. These voltages are

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	PEFERENCE DESIGNATION	No.		CRIPTION		WIL SPEC OR MEG.	MIL TYPE OR MEG. PART NO.
		X		daterial Mod. 10	Control		49-200-493-501
	R. 3, 4, 6, 26	5				Wil-R-2568	RT.07AD222J
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	28 5						
			Residior		Fixed Film, 4.78,5%, O.E5W.	M11-R-22684	R.L07AD472J
, "	R 32, 35,34, 36	4	Res 1000r	Fixed Film,	Fixed Film, * 15%, 0.25%.	Mil-R-22684	RL07AD
- 0	RIO. 12. 16.	e	Resido	Resider. Fixed Film, 3,34 5%. 0.25 W.	* 5%. 0.25 W.	M11-R-22684	RI.07AD332J
	R20,23	.2	Resistor	FIXED FILM 2	224 5%, 0.50W.	M11-R-22684	Rt.20 AD220J
œ	R 19, 30	Ŋ	Reststor,	Fixed Film,	0K + 5% 0,25W.	M11-R-22684	RL07AD103J
	R29		Restator,	., Flxed Film 2K	K + 5%, 0, 25W.	Mil-R-22684	RL07AD202J
£	X		Resistor	r. Fixed Film, \$704.5% .,25W.	7245% .,25W.	M11-R-22684	RL07AD471J
=	0ID		Capacitor.		Tantalulu Folur 330 uf. 6V.	MILC-26655B	CS13BB337K
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	7 ZEAMIN	TERMINAL TURKET	03350	2030B
	AR WIRE AWG TEG	WG#26 TYPEB	M12-W-16878D	ALPHA #1853
	AR SOZDER SNEC	SHED	125-8-00	TYPE PA
	14R 12/21		95281-7-7W	TYPE A
	AR CONDUCT	CONDUCTOR SOLID ANG ES	EVE 11-00	BELDEN BORZ
	AR SHRINK TUBING	TUBING RNF-100	MSEC-SPEC-276	276-11 TOD 05 DVA
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NOTES:

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1. PRINTED CIRCUIT ASSEMBLY TO BE CONSTRUCTED AND INSPECTED PER NPC 200-4

2. ALL TERMINALS SHALL BE MOUNTED ON THE PRINTED CIRCUIT BOARD PRIOR TO INSERTING ELECTRICAL COMPONENTS

- 3 TERMINAL IDENTIFICATION PART & PLUG NUMBERS ARE TO BE APPLIED IN BLACK INK . 12 INCH HIGH IN POSITION SHOWN
- 4. COAT ALL TERMINALIDENTIFICATION, PART, & PLUG NUMBERS WITH CLEAR LACQUER
- 5. AFTER QUALITY CONTROL HAS TESTED AND ACCEPTED THE PRINTED CIRCUIT ASSEMBLY APPLY A CONFORMAL COATING TO BOTH SIDES OF BOARD COATING MUST COMPLY WITH MSFC-PROC-257
- G REFERENCE DWG.

 PRINTED CIRCUIT BOARD 49-300-543-001

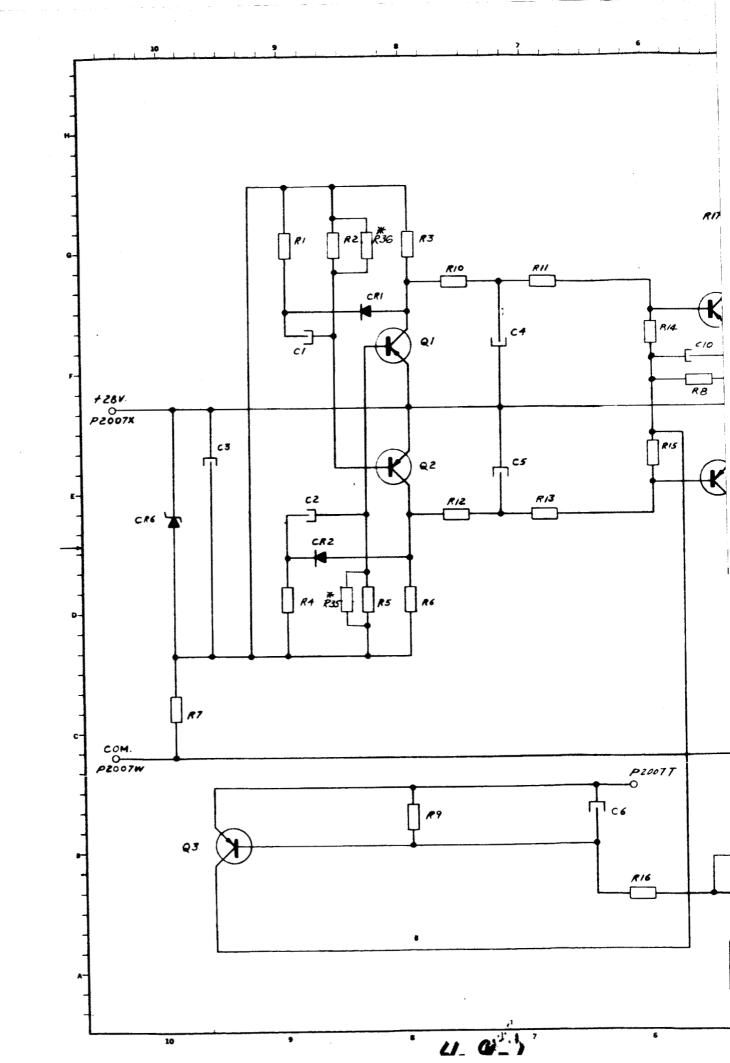
 PRINTED CIRCUIT MASTER 49-300-543-091

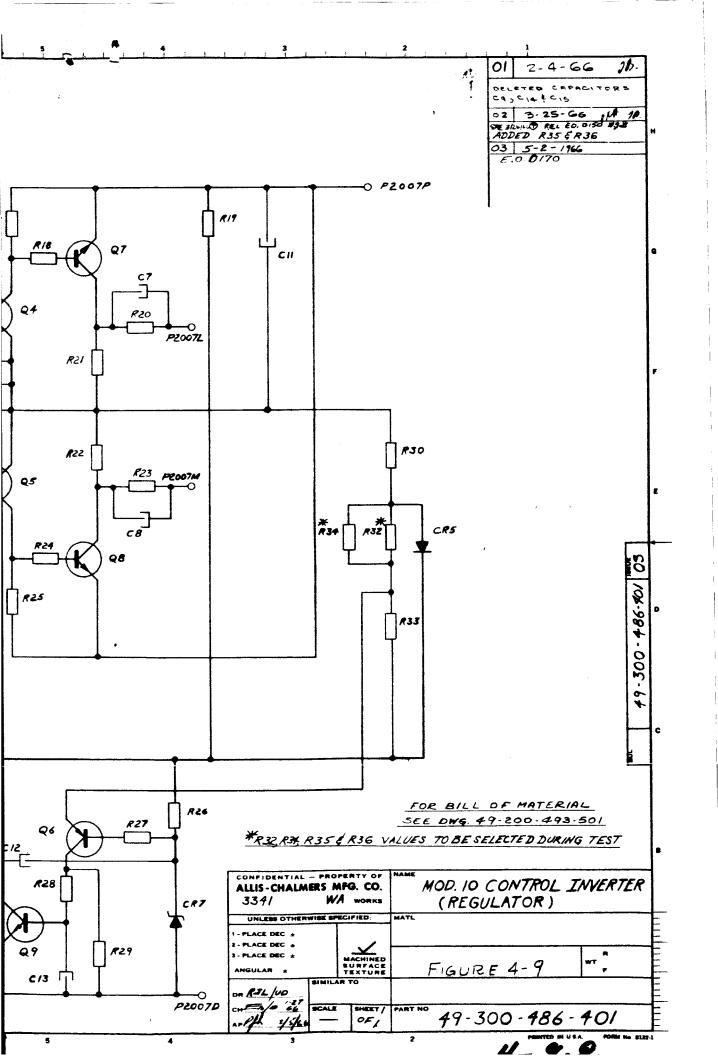
 ELECTRICAL SCHEMATIC 49-200-486-401

49-200-493-501 NEXT ASSEMBLY USED ON CONFIDENTIAL - PROPERTY OF ALLIS-CHALMERS MFG. CO. PRINTEL CIRCUT ASSEMBLY 3341 MI WORKS CONTROL INVERTER UNLESS OTHERWISE SPECIFIED: - PLACE DEC ± 2-PLACE DEC ± .0/ - PLACE DEC ± MACHINED SURFACE TEXTURE FIGURE 4-8 ANGULAR DA (UDC) 3:1 49-300-542-401

² #1058 (UDC)

POPE No. 0112





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	Make From Glass Epoxy	COC COMP COMP COMP		
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CSI3AE101K	NIL-C-26655A	Capacitor, Tantalum Polar 100mf 15V.		10 02
1300117C2050W2		Capacitor, Tantalex 110uf 50V.	4	6
49-200-490-401		Output Choke	7	8 7.8
49-200-489-401		Input Choke &	7	7 T-2
49-200-491-401		Transformer	7	6 1-1
IN3041B		Zener Diode 75V		5 CR3 [14.15
IN4003		Diode	14	4 8.9.10.11.12.13
20805 - 1	USRCO	Terminal	23	
2500C -1	n/sico	Terminal-Feed Thru	22	
49-300-501-001		1 Circuit Board		
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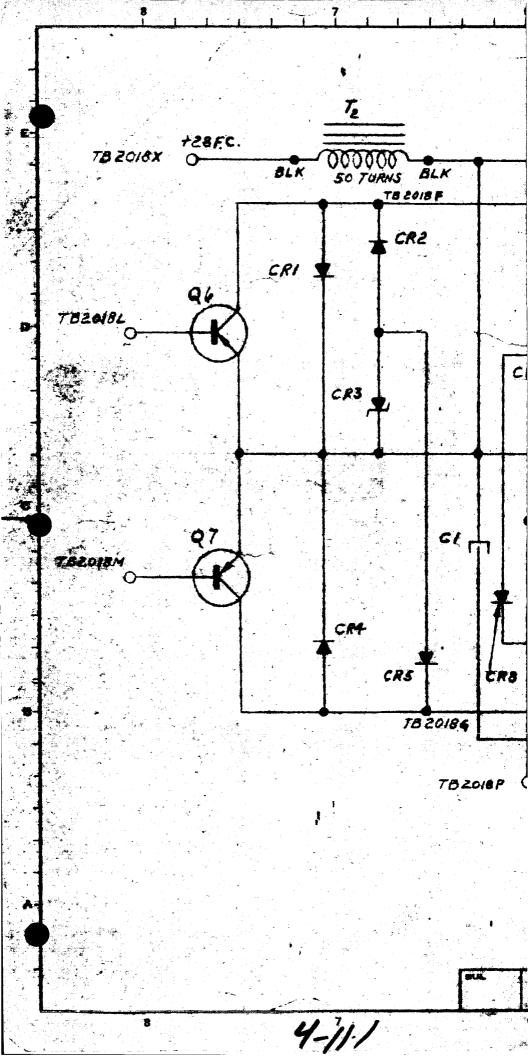
49-200-492-014

2 Washer-0.50 O.D.x0.125 I.D.x.093rhe From Glass Epoxy 49-200-492-013

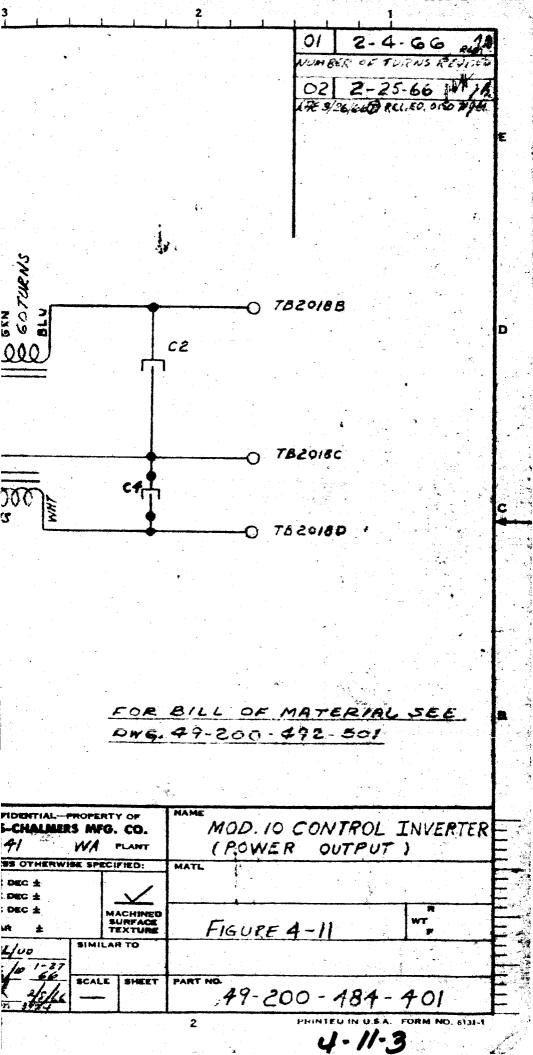
No.6-32x1.25 Lg. Mach. Screw No.6-32x1.00 Lg. Mach. Screw

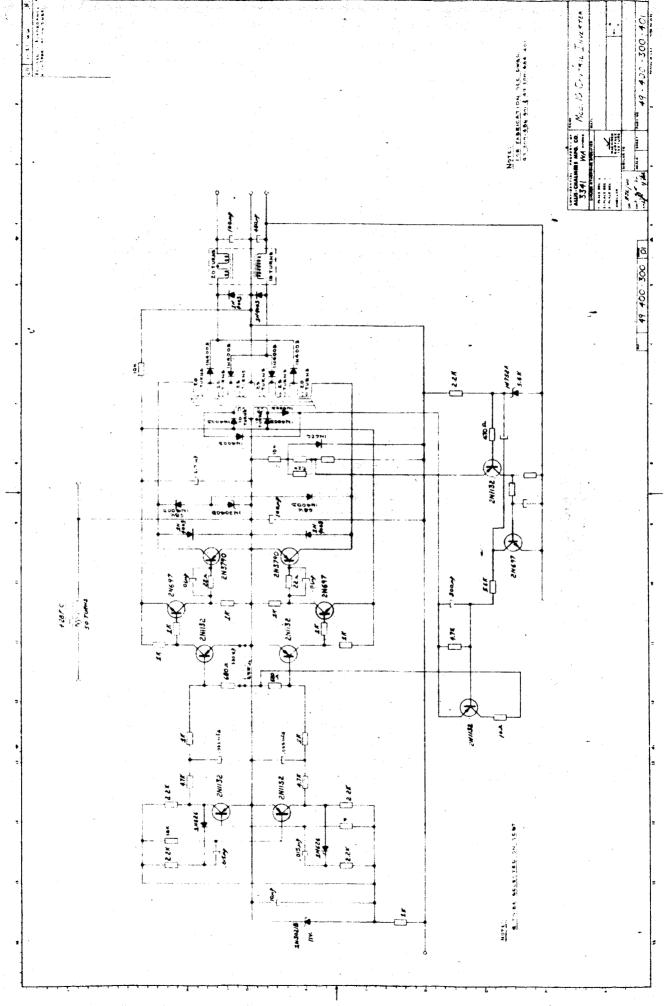
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7	က	No. 6 Lockwasher	00-655-017-018
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19	2 '8"	2'8" #22 AWCIFE Teflon Insul. Stranded 2'8" Silver Plated Copper Type E - White Mil-W-16878D	Alpha 2855 or Equivalent
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supplied by a dc. to dc. inverter from the auxiliary 28 volts dc. power source which may be either the fuel cell output or an external source. The control power supply is designed to operate over an input voltage of 18 to 35 vdc with an overall efficiency of not less than 70% at a 28 volt input. The power supply operates as follows. The output of an 800 cycle, free running, square wave oscillator, is modified to a triangular wave. The triangular wave drives an amplifier into saturation over approximately 165 electrical degrees. The output of this amplifier drives a transformer which operates similar to an AUTO transformer being alternately switched across the dc. power source. One secondary winding provides power for the 11.2 vdc filter network. Another secondary winding provides the power for the -5.6 vdc filter network, which in turn feeds the main voltage regulator circuit. A reactor forms part of the filtering network of both the +11.2 and the -5.6 vdc outputs. It acts as a load equalizer for any unbalanced load currents between these two outputs. The main voltage regulator circuit controls the bias applied to amplifier, thereby providing pulse width voltage regulation.

4.5.2 <u>Temperature Controller</u> See Figure 4-13A and 14-13B (Dwg. No. 49-200-413-501), Fig. 4-14 (Dwg. No. 49-400-337-401), Fig. No. 4-15 (Dwg. No. 49-400-293-401).

The temperature controller consists of 3 distinct circuits: the sensing circuit, the coolant circuit, and the heating circuit. The sensing circuit determines whether cooling or heating is required by sensing the fuel cell stack temperature. It then provides a signal to either the coolant control circuit or the heating circuit, which control respectively, the liquid coolant control valve or the fuel cell stack standby heaters.

The temperature of the fuel cell stack is monitored by a thermistor located on the stack. This signal is fed to an operational amplifier whose output is

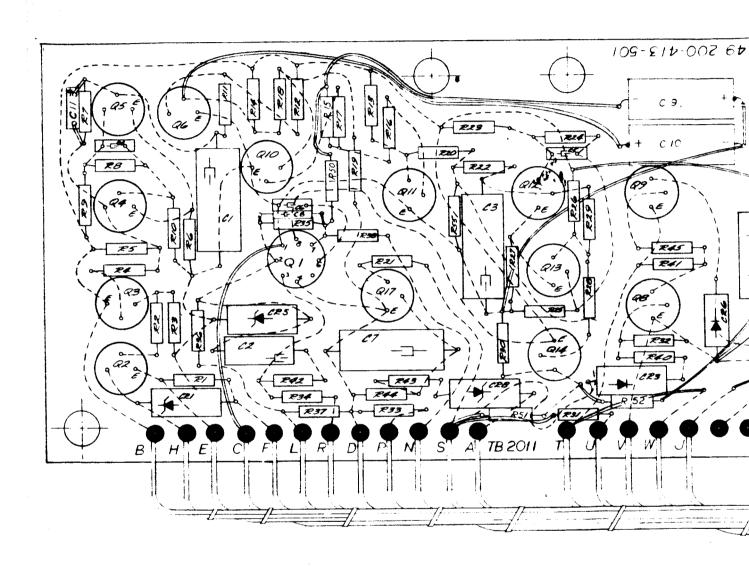
u 1			2		
	CIRCU	ΙŢ	CIRCUIT COMPONENT LIST FOR DRA	DRAWING 49-400-337	-401 MX
NO.	. REFERENCE	NO. REQ.	DESCRIPTION	MIL SPEC. OR MFG.	MIL TYPE OR MFG. PART NO.
-	R34,36 R1, 2, 9, 23,	Ø	Resistor Fixed Film, 212K+5% 0.25W	MIL-R-22684	RL07AD222J
2	R3, 11, 5 5		Resistor Fixed Film, 5.6K + 5%:0.25W	MIL-R-22684 ·	RL07AD562J
~	R4, 2 , 16, 17, 12, 28, 33, 37, 44 43	6	Resistor Fixed Film, 10K + 5% 0.25W	MIL-R-22684	RL07AD103J
4	R5, 26	2	Resistor Fixed Film, 1.8K - 5% 0.25W	MIL-R-22684	RL07AD182J
ເດ	R6, 27	2	Resistor Fixed Film, 220 ohms - 5% 0, 25W	MIL-R-22684	RL07AD221J
9	R7, 29, 32, 35	4	Resistor Fixed Film 100K 15% o. 25W	MIL-R-22684	RL07AD104J.
- /e	R8, 24	2	Resistor Fixed Film 8,2K + 5% 0,25W	MIL-R-22684	RL07AD822J
3 A	R10, 25	7	Resistor Fixed Film 6,2K + 5% 0,25W	MIL-R-22684	RL07AD622J
6	R30, 22, 53, 51	A	Resistor Fixed Film 2K - 5% 0, 25W	MIL-R-22684	RL07AD202J
2	R31, 18, 21, 54, 42	N.	Resistor Fixed Film 1K + 5% 0, 25W	MIL-R-22684	RL07AD102J
==	R45	-	Resistor Fixed Film 4, 7K + 5% 0, 25W	MIL-R-22684	RL07AD472J
1.2	R15, 52	ત્ર	Resistor Fixed Film 3, 3K - 5% 0, 25W	MIL-R-22684	RL07AD332J

	•	R41	-	Resistor Fixed Film 5.1K + 5% 0.25W	MIL-R-22684	RL07AD512J
	74	R40	1	Resistor Fixed Film 20K - 5% 0, 25W	MIL-R-22684	R L07AD203J
	15.	R30, 14	7	Resistor Fixed Film 12K + 5% 0, 25W	MIL-R-22684	RL07AD123J
	16	K1	-	Relay Permanent Magnet 24VDC	P&B	SCIIDB
	17	C2	-	Capacitor Geramic 22.00pf	MIL-C-11015C	CK06CW222K
	18	C4, 5	2	Capacitor-Ceramic 470pf	MIL-C-11015C	CK05CW471K
ü	19	C6	-1	Capacitor Ceramic 1000pf 200V	MIL-C-11015C	CK05CW102K
	2.0	C1, 3	2	Capacitor Tantalum Polar 10mf 35V	MIL-C-26655	CS13AF100K
	21	C7,10	2	Capacitor Tantalum Polar 47mf 35V	MIL-C-26655	CS13AF470K 1
	22	CR1		Diode Zener 39V		IN3034B
	23	CR3,	1	Diode	MSFC-338/3	SIN626
4	24	CR6	1	Diode		IN4003
-/E	25	CR 5	1	Diode Zener 3.6V	MSFC-338/8	SIN747A
5 A	92	CR8		Diode Zener 6.8V	MSFC-338/8	SIN754A
1	27	01		Operational Amplifier	Fairchild	MA702A

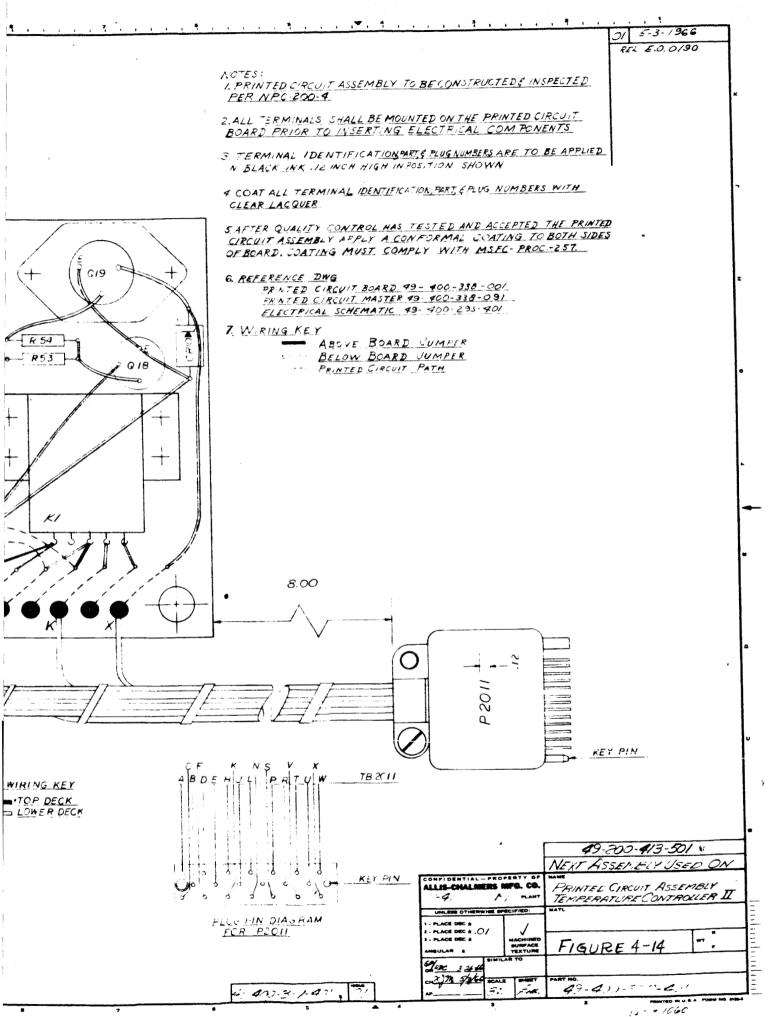
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	FIGURE 4-134	FIGU	y of		P. 4.	1.3-De.	15 2K (17.9)	7
			₩	DECIMAL #	צון	10000 10000	10 K (17.8)	
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1 .	CKOGCWI52K	0150	M1L-C-110	CERAMIC 1500 pf	CAPACITOR C	_	8	₩ 4
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	RECORD 4713	684	MIL- R- 22	160 FILM 470.0 15% 0.25W	RESISTOR FIXED	-	유 0 전	ଶ
F	RLOJAD 682J	489	MIL- R- 22	FIXED FILM 6.8K 15% 0.25 W	RESISTOR FIX	-	R20	7 32
		e con design in the design in		SELECTED DURING TEST	*VALUE SEI			
1	*	2684	MIL- R. 2	FIXED FILM * TS% 0.25W	RESISTOR FIX	ત્ર	R19 , R13 *	30
1	\$ 2N1132	8	MSFC-338/108		Transistor	4	03, 9, 10, 14	59
*	\$2N6 97		MSFC-338/105		Transistor	9	12, 13, 17, 18	28

'					
	REO.	REO. LTEM	DESCRIPTION	MIK. STACOK MIKE.	PART N MBER
•	1	4.0	pad Translator Mounting	Transipad Products 100-12DAT-Black	100-12DAT-Black
·		ı		(11ton Ross	10229
	23	1		USECO	, 8080Z
<i>-</i>	· V	4.3	Wire AWG 26 Type B	1/82891-M-111	Alpha #1853
.A	Ä	4.4	Solid AWG #24	99-W-99	Baldan #8022
	AR	45		MSEC-SEC-516	276-11T0D05 DIA
	AR	46		00-8-571	Type 3A
	A R	4.7		MIL-F-14256	Type A
4	-	8.4	Printed Circuit Board		49 400 338 001
	ي	49	We Transfer	MS-51957	MAE1950-14
13	ور	50	Nut Salf Locking	NAS1021	NAS 1021004
2	ی	5.	Washer Plain	MS-15795	MG18795-804-804
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2		ASSEMBLY USED ON 49-200-585-502		
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	Ref	Electrical Schematic	49-400-293-401	
13-8		SHOUL CELTS. ALLIS-CHALMERS MFG. CO. ** *********************************	Temperature Costroller M&C 10	
3				
			49-400-413-50c	

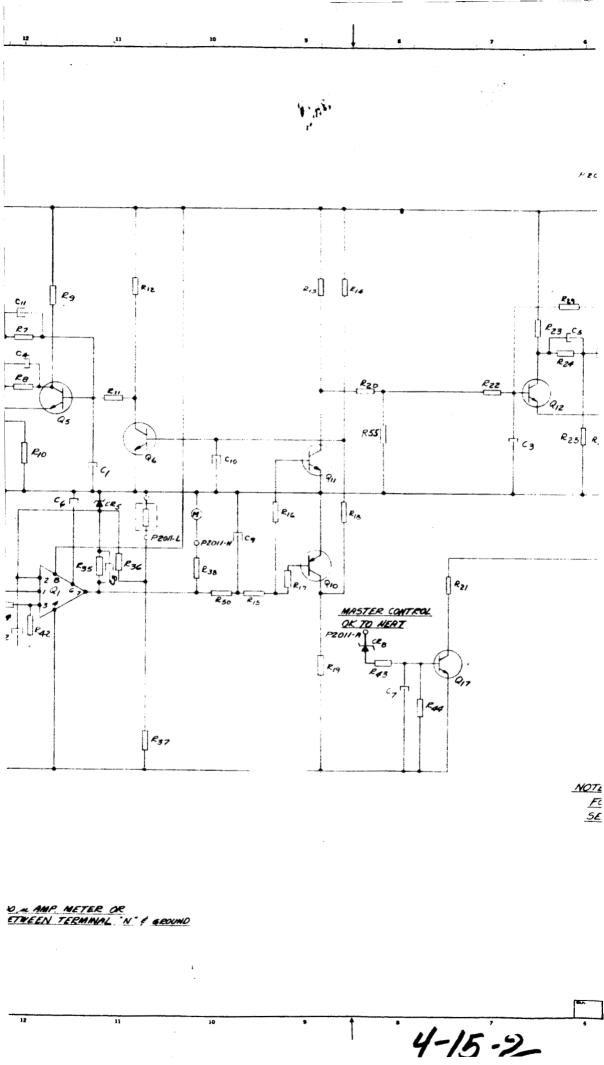


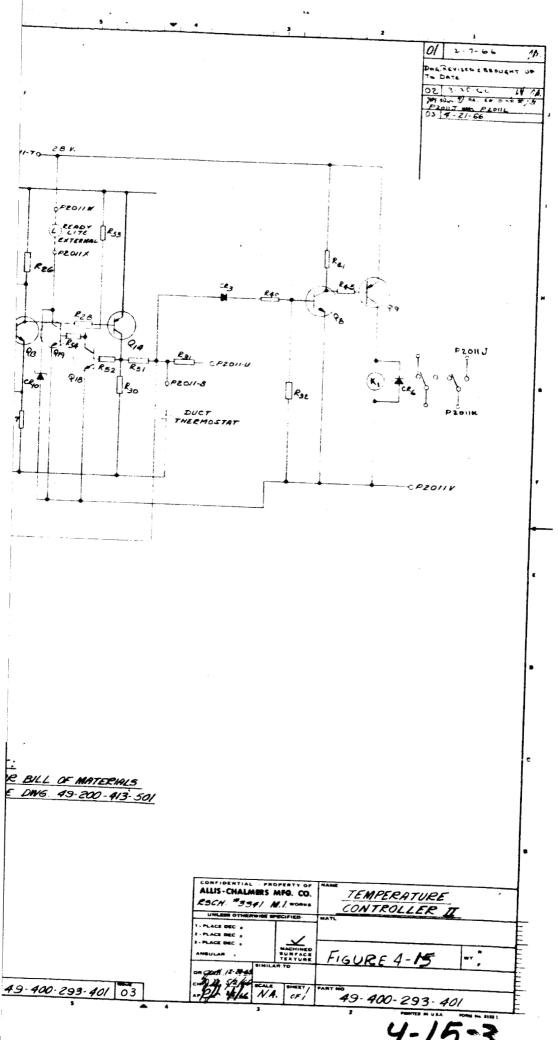
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+ /1.2 VDC P2011-B 0-PZOII-C 0-P2011-P -5.6 VDC F 2011-D EXTERNAL COMPONENT EITHER AN EXTERNAL 500-0-5

4-15-





a negative signal if cooling is required, or a positive signal if heating is required. The positive signal from the operational amplifier is fed to an inhibited AND gate. To satisfy the inhibited AND gate, the "OK to Heat Signal" from the master controller must be present, the "Stand by heater thermostat signal" cannot be present. Completing the input requirements of this gate, the output feeds a Schmitt trigger with dual outputs: one turns on the 100-watt current driver (100 watt supply for the standby heaters), the second output is the command signal for the 1,600 watt warm-up heaters. The negative signal from the operational amplifier feeds the coolant Schmitt trigger circuit which in turn triggers the relay driver for the coolant control valve.

4.5.3 Purge Controller - See Figure 4-16A and 4-16B (Dwg. No. 49-200-465-501), Fig. 4-17 (Dwg. No. 49-500-183-401), Fig. 4-18 (Dwg. No. 49-400-291-401).

Purging is accomplished by a brief and accurately timed opening of the purge valves which permit a rapid movement of hydrogen and oxygen through the respective reactant cavities of the fuel cell. This action cleans the cavities of inert gases which are an accumulation of impurities contained in the reactant gases. It is therefore evident that the frequencies of purging are related to the amount of reactant gases used and the amount of impurities in the gases. The amount of reactant gases used is directly related to the ampere-hours of current produced by the fuel cell.

The purge controller provides three modes of purging.

Angele and the second s		and the state of t	Comments of the contract of th			
	CIRCL		4 54 F	DRAWING 49-500 183-401	The second secon	
E.S	REFERENCE	NO.	DESCRIPTION	MIL SPEC. OR MFG.	MIL TYPE OR MFG. PART NO.	
	1		Resistor Fixed Film St.A. 15% 0.25W	MILLE DE COMPORT	2013072071	.
	R2 3 141.6	4	Besistor Cixed Film 2.2x 15% 6.25%	21 - 2-2039 F	CONTRACTOR AND CONTRA	
	The state of the s		Resistor Fixed Film 821152 0.257	MIL 1 - 3 - 32 6 9 0 1	91.07AT 82.3.7	
5	- 810 140R1	67)	Resistor Swed Film 1K-5% 0.25W	W15-0-22684/	11.07.AD.1.62.L	
ما جر	\$ 6 A	7	Resistor lixed Tim 12r 3% o.25%		71,02001233	130
		- Committee of the Comm	Resister lixed Fill 100 A 58 0.25W	MIN 9-22684/	The Control of the State of the	
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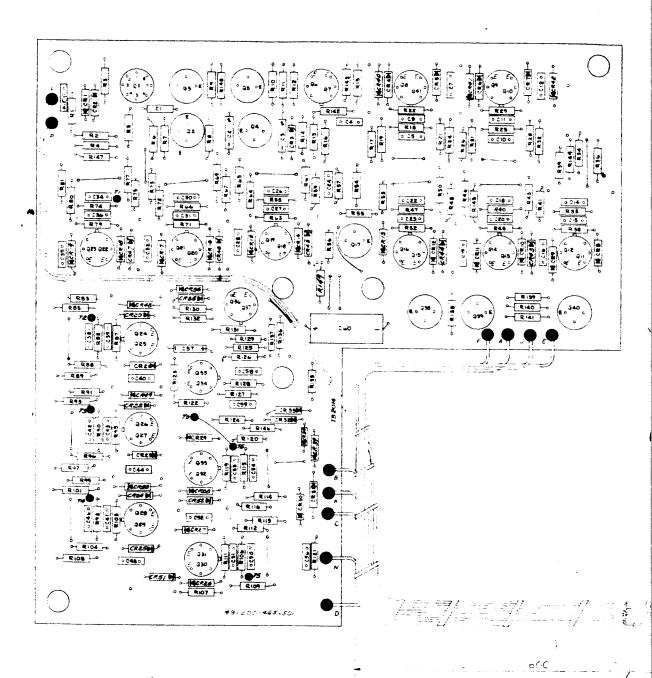
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	TA 21 8 10 810		Resistor Fixed Film A.7X15% 0.35W	VII. 11-22004/	BL07AD472.1.
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		2.9	Residence Fixed Tilm 22K+5% 0.25W	M11-R-22684/	N. 67.40223.1
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10. 8CALK 2712	MI DEPT SIMILAR TO	3341	PIX. Ref. Dec ut Kon	Separation of the separation o
FIGURE 4-16A	- Property of CO., Milwaukee, Wis.	ALLIS-CHALMERS MFG. CO., Milwaukee, Wis.	12 S 1 2 S 1 S 1 S 1 S 1 S 1 S 1 S 1 S 1	(47.6.); R 13 + (17.9); R 12 = (17.10); C 56 (17.14); G, 9, 13, 19, 19, 25, 27, 38, 38, 38, 38, 38, 38, 38, 38, 38, 38
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materia ya sa			Capacitor, Caplalue 68 uf	MIL-C-26655 /2	
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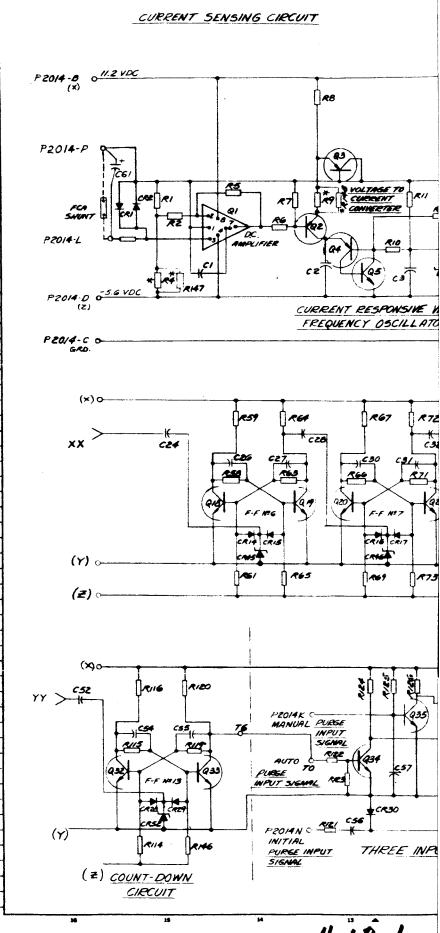
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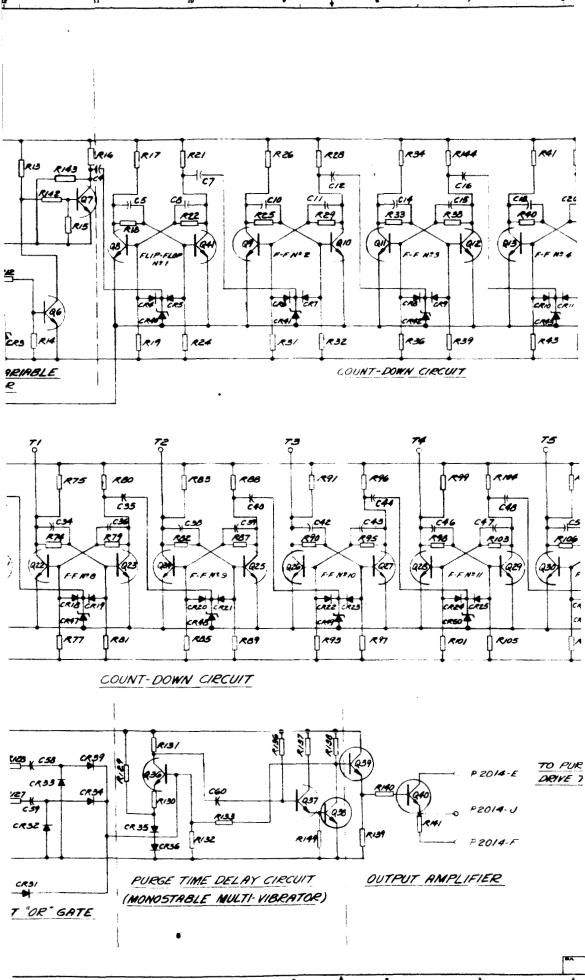
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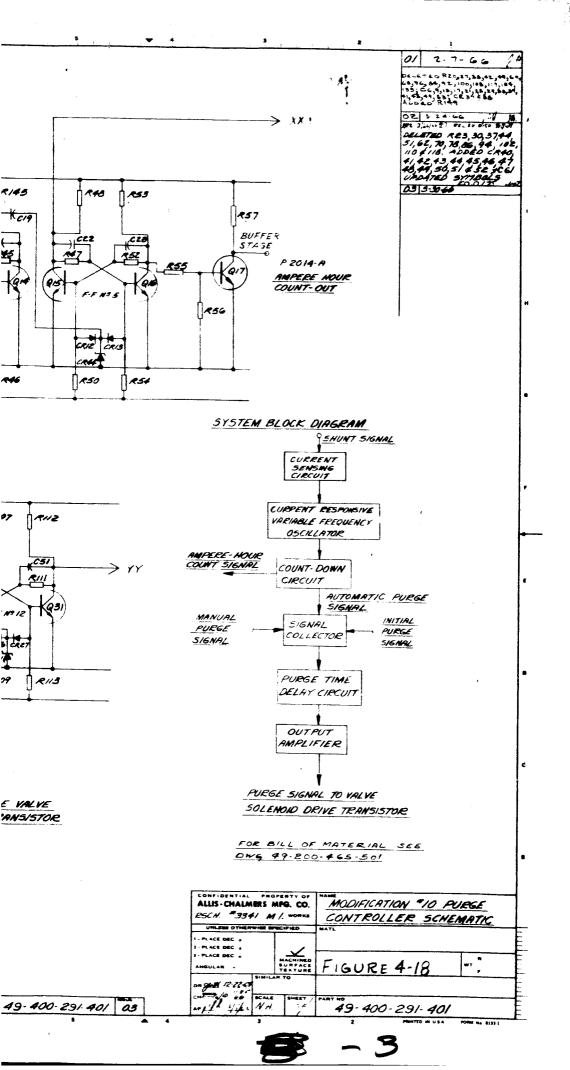
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Normal Operation - Purge cycling during normal operation is controlled by the ampere-hours (AH) of current delivered by the fuel cell. The load current signal from the fuel cell shunt is processed in a differential amplifier which provides a linear voltage to a relaxation oscillator and pulse circuit whose output pulse rate is directly proportional to the fuel cell output current. However, this pulse rate is too high to be of practical value. Therefore, this output is processed through a binary counter string which consists of a series of flip-flops until a predetermined output rate is obtained. The pulse circuit is normally adjusted for approximately four pulses per AH at the input to the binary counter string. Outputs obtained from successive flip-flops are two pulses per AH, one pulse per AH, one pulse per 2 AH, etc. until one pulse per 256 AH is obtained at the end. The purging rate is preset by selecting the appropriate tap of the binary counter string. This selected output is fed to an QR gate which feeds the delay monostable multivibrator energizing the purge valves through the valve driver. The duration of the purge is dependent upon the circuit parameters of the monostable multivibrator.

Manual Operation - If desired, a manual purge can be initiated by depressing the purge push button which supplies a trigger pulse to the OR gate circuit.

Automatic Purge at "APPLY LOAD" - When an "apply load" signal is applied to the EMCS, an initial purge signal is sent from the master controller to the OR gate for accomplishing an initial purge whenever load is first applied to the fuel cell.

4.5.4 Moisture Removal Controller - See Figure 4-19A & 19B (Drawing No. 49-200-454-401), Figure 4-20 (Drawing No. 49-300-545-401), Figure 4-21 (Drawing No. 49-200-421-401).

The moisture removal controller maintains the desired KOH concentration in the fuel cell stack by removing the excess by-product water produced by the reaction. Because the percentage of KOH concentration is a function of the moisture removal cavity pressure and the stack temperature, these two parameters are used as the controlling functions.

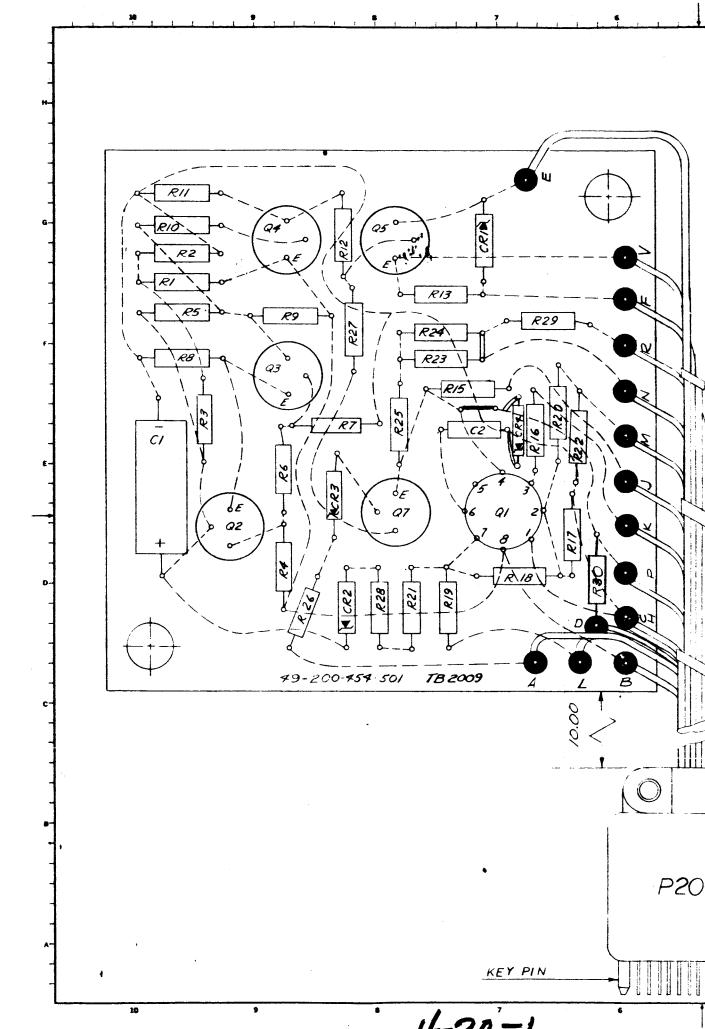
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		CIRCUIT		COMPONENT LIST FOR DRAN	ST FOR DRAWING 49-300-575-70/	
	REFERENCE DESIGNATION	NCE	NO. REQ.	DESCRIPTION	MIL SREC. OR MFG.	MIL TYPE OR MFG. PART NO.
	R20 720		•	Registor Fixed Film * + 5% 0, 25 W	ML-R-22684	
	×			Registor Fixed Film 2K + 5% 0.25 W	MIL-R-22684	R L07AD202J
	$\mathbb{R}_4 \times \mathbb{R}_2$	R_{13} R_{11}	7	Resistor Fixed Film 2.2K +5% 0.25W	MIL-R-22684	R L07AD222J
	2			Resistor Fixed Film 100K + 5% 0.25 W	MIL-R-22684	R.L07AD104J
	R6, R1		તાં	Resistor Fixed Film 8.2K + 5% 6.25 W	MIL-R-22684	RL07AD822J
9	7			Resistor Fixed Film 6.2K + 5% 0.25 W	MIL-R-22684	R L07AD 622J
	R 8		-	Resistor Fixed Film 220 + 5% 0.25 W	MIL-R-22684	RL07AD221J
. a	4			Resistor Fixed Film 1.8K + 5% 0.25 W	MIL-R-22684	RL07AD182J
9	Rice R	19	2	Resistor Fixed Film 12K +5% 0.25 W	MIL-R-22684	R L07AD123J
0	-		-	Resistor Fixed Film 5.6K ±5% 0.25 W	MIL-R-22684	RL07AD562J

	A15, B17		. 7	Resistor Fixed Film 5.1K + 5% 0.25 W	MIL-R-22684	R L,07AD\$123
	R 18			Remistor CARBON 330K + 5% 0.25 W	MIL-R-11/8	RC07GF334J
	R20			Resistor Fixed Film 22K + 5% 0.25 W	MIL-R-22684	R LO7AD223J
c	R22 , R25	25, R 26	"	Resistor Fixed Film 10K ± 5% 0.25 W	MIL-R-22684	RLO7AD103J
	I So			Resistor Fixed Film 470 + 5% 0.25 W	MIL.*R.22684	RLO7AD471J
	Roy			Wesistor Fixed Film 820 + 5% 0.25 W	MIL-R-22684	R LOTAU821J
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	S S		7	Capacitor, Ceramic 1900 pf	MIL-C-11015	CK05CW102K
		を持つ		Diode, Zener		IN3032
	G S S	22 19 7 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	J.	blode Zener 3,6 V	MSFC-236/8	SIN747A
	CR3		oh;	V8.8 V	M\$FC-338/6	SIN754A
	ď			Operational Amplifier	Fairchild	uA-702
	0,00	, 0 0 0		10181810	MSFC-338/105	\$2N697
					MSFC-338/108	\$2N1132
					WINDHESTER	SMCE-20- 46H

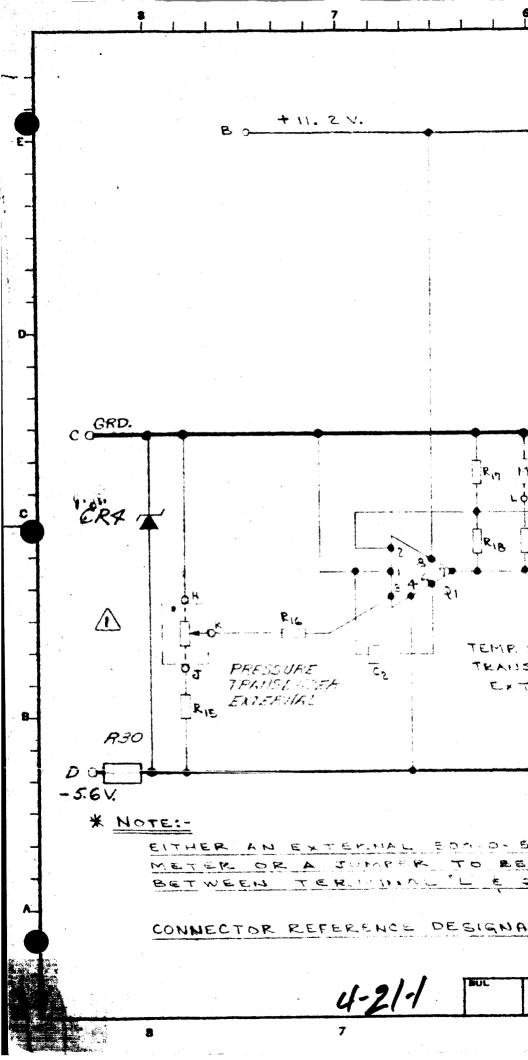
F.		R3D			Resistor Fixed Fi		01 +5% 0.25W	25₩	N11-R-22684		RI,07AD 510.1	Augus
e Maria					FND TRA	NSISTON	END TRANSISTOR MOWTING		TRANSIA PROLIDE	PROLIDE		
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en version in				\$	WIRE AWG	4WG#2	#26 TNPE B		M12-W-16873D	22	41744 #1853	
	Ŋ			X	\$207K	15			125-5-00		TYRE RA	
G				X					ML-F-14256	28	TYPE A	
				4	SWRINK TUBING	748WG	÷.	3	RME LOC MSFC - SPEC 276	. 542	276-1170DOSDIA	NA NA NA NA NA NA NA NA NA NA NA NA NA N
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4		4 K 4			DIODE,	RENE	DIODE, BENER 3.1V				NN 75/4	
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								14. S		V.	49-200-4 54-501	

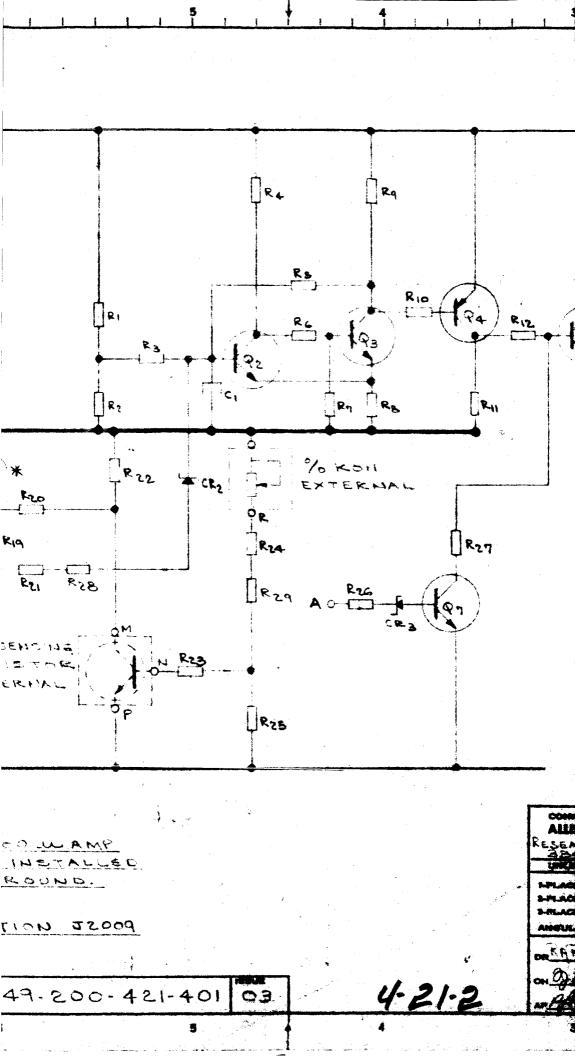
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		CIRCUIT		COMPONENT LIST FOR DRA	IST FOR DRAWING 49-300-545-401	x12108-50
	- ON	REFERENCE DESIGNATION	NO. REQ.	DESCRIPTION	MIL SPEC. OR MFG.	MIL TYPE OR MFG, PART NO.
A	37	82	/	RESISTOR FIXEDFILM IK ESTO	MIC-R-22684	REOTAD 102J
	38		AR	LACING TAPE, BLACK	MIL-T-213A	ALP44 #20134
В						
						The address of the control of the co
	7					The state of the s
<u>b</u>	7	10				
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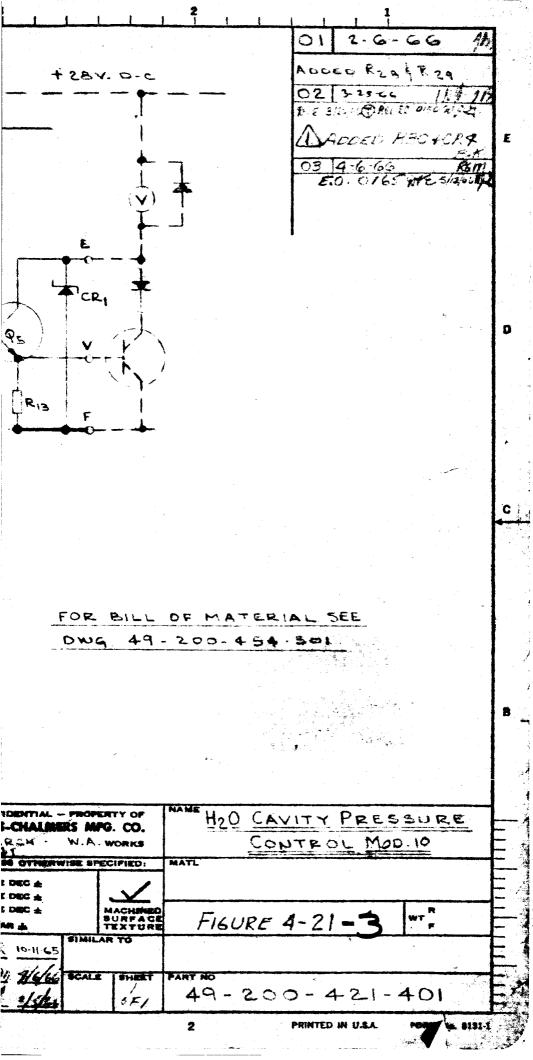
419-B - 2- 8-61-8 80.5 19-66 18 18 18 18 18 18 18 18 18 18 18 18 18	A.C. Marie Constant and the P. Solomon of H. S. Solomon		, E	, , , , , , , , , , , , , , , , , , ,			
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NOTES:							۳
1. PRINTEL C	IRCUIT ASSET	BLY TO BE C	ONSTRUCT	FL AND			
NSPE 15	E PER NP	C-200-4					
2.ALL TERI	MINALS SHA	LL BE MOUN	ITED ON T	HE PRINTED			
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				49- 300-54 49-300-54			Į
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	PRINTED C	IRCUIT PA	TH			6	
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	PLUG	PIN DIAGRAI	<u>u</u>				
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		<u> </u>		NEXT ASSEM	BLY USED	ON	
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	2	1-PLACE DEC ±					
.12	ı	2-PLACE DEC ± ,O	MACHINED	<u> </u>	4 00	WT R	-
<u></u>	•		SURFACE TEXTURE SIMILAR TO	FIGURE	4 - 20	<u> </u>	
		CHA 1 1/5/4	SCALE TOURS	PART NO			=
		AP	3.1 FINAL	49-300-	145-401	·	=
5	4	3		2 1054-UDC			_







Stack temperature is sensed by a transistor embedded in the fuel cell stack. The temperature-emitter current characteristic curve of this transistor closely matches the KOH concentration temperature - vapor pressure characteristic curve. The output of this transistor provides a reference voltage signal of the stack temperature. The moisture removal cavity pressure is sensed by a variable resistance type transducer mounted ahead of the moisture removal solenoid valve. The transducer provides a voltage signal proportional to the actual moisture removal cavity pressure.

These two signal voltages are applied to a differential amplifier. If a negative output signal is present, the pull-in coil of the moisture removal solenoid valve relay will be energized through the action of the control amplifier. The magnitude at which the valve operates is determined by the desired allowable pressure error band. A transistor interlock is provided to prevent actuating the valve unless the load has been applied.

4.5.5 Master Controller - See Fig. 4-22 A and 4-22 B (Dwg. No. 49-200-456-501), Fig. 4-23 (Dwg. No. 49-500-184-401), Fig. 4-24 (Dwg. No. 49-300-474-401). The master controller distributes the input control signals to the proper circuits and functional devices, and integrates protective controls into the fuel cell systems. The master controller operates as follows:

Under normal startup conditions, the start AND gate must have present -5.6 VDC, +11.2 VDC, +28 VDC, and the start command. Having satisfied these conditions, an "OK signal to heat" is sent to the temperature controller which turns ON the stand-by heaters and commands the warm-up heaters to be turned ON.

			4	
	CIRCU	CIRCUIT COMPONENT LIST FOR DRAWING	DRAWING 49-500-181-401 PIX	-491 PIX
	IT. REFERENCE NO. DESIGNATION	NO. DESCRIPTION	MIL SPEC. OR MFG. NAME AND CODE	MIL TYPE OR MFG, PART NO.
A A	L. R. 26, 36, 67, 79	4 Resistor Fixed Film IK ± 5% 0,25W		
	2 8 8 8	2 Resistor Fixed Film 1, 5K + 5% 0,25W		RTO7AD 192J
	3 IX 13, 23, 31.	-8 Resistor Fixed Film 1.8K ± 5% 0.25W		RLOZAD 1821
	.13. 59, 66, 74, 85			
	4 . K 16.18. & 5.3	., R. 16. 18. & b3 3 Resistor Eined Film 2, OE ± 5% 0, 25 W	21.W MILL-R-22684	. RLOTAP 2021
	5. 18. 19. 25, 31.35	5 R. J. 12, 25, 34, 35, 14 Resistor Fixed Film 3, 3K & 5% 9, 25W	.5W MII -R-22684	RLO7AD 222J
	38, 46, 47, 55, 58,		The second secon	
· · · · · ·	. 3 4 69.77.80, b 38.		A second of the	
- 9	20 R 11, 8, 54	& Resistor Fixed Filter 3, 317 4 cm 0, 25 W.	5 W MIJ-R-22684	RLOTAP 332J
3 P	7 B 33, 45, 76, 87	1 Resistor Fixed Film 5, 6E + 35 0, 25W	25 W MILL-R-22684	RLOZAD 562J
1.7	B. R. 29, 41, 72, 83	. 4Resistor Fixed Vilm e, 2K, 4 .5% 0.25W	5W MIL-R-22684	RLO7AD 6223
	9 R 6 9 23 40	Z. Resistor Fixed Film 8, 2K, 1-5% 0, 25W	5W 1 MU-R-22684	RLO7AD 822J

	50, 71, 82				
=======================================	R 2. 3.17.49.20	.=	Resistor Fixed Film 10K 1 5% 0, 25W	MIL-R-22684	RLO7AD 103J
	48.49.52.56.57				
	62				
	R 14, 22, 32, 44				
		82	Resistor Fixed Film 12K ± 5% 0.25W	MIL-R-22684	RLO7AD 123J
12	R 24, 37, 51, 68,	40	Resistor Fixed Film 22K ± 5% 0.25W	MIL-R-22684	RLO7AD 223J
	78, 21				
13		-	Printed CIRCUIT Board		49-400-342-001
2	R 10 27 39 53	œ	Resistor Fixed Film 100K 1 5% 0.25W	MIL-R-22684	RLOTAD 104J
	70. 81. 15. 61				
्र र		2	Transistor Pad	MILTON ROSS	10229
16	R 30, 42, 73, 84	4	Resistor Fixed Film 220mt 5% 0, 25W	MIL-R-22684	R LO7AD 221J
12	R 4 W 7	~	Resistor Fixed Film 1202 + 5% 0.25W	MIL-R-22684	RLO7AD 121J
18	R 86	1	Resistor Fixed Film 56K ± 5% 0.25W	MIL-R-22684	RLO7AD 5633
2	R 89	-	Resistor Fixed Film 5.1K 1 5% 0,25W	MIL-R-22684	RLO7AD 512J.
9	C 1 3 4 10 1113	. 4	Capacitor Tantalum 0. 33 mt	MIL-C-26655B	CS13BF334K
77	C 7 9 16 18	4	Capacitor Tantalum 10 mf	MIL+C-26655B	CS13BF106K
22	C & R 15. 17	4	Canacitor Tantalum 68 mf	M11C-26655B	. Xysyabey

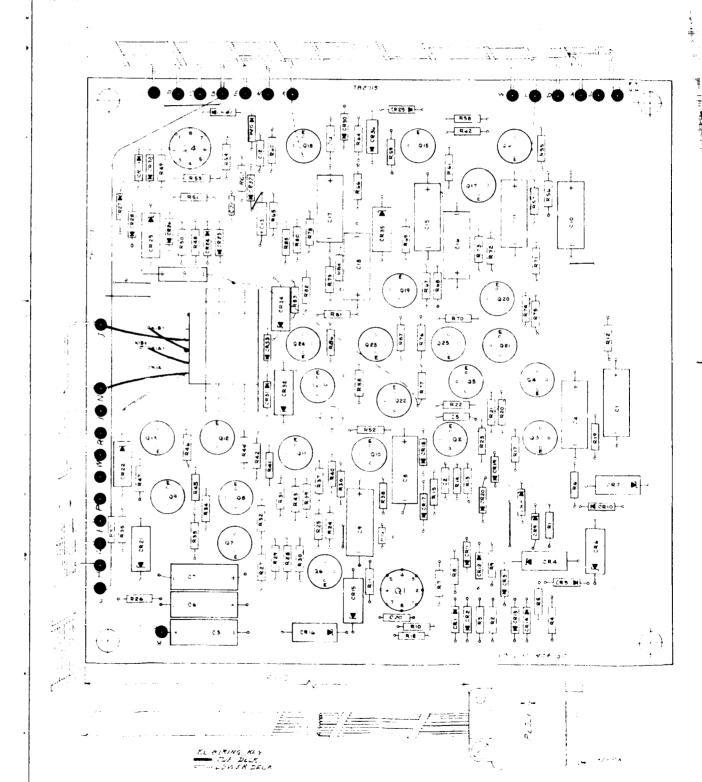
222	Capacitor Ceramic 220 pf	MIL.C. 11015	CK05CW221K
24 @ 1 & 14 2 2	Operational Amplifier	Pairchild	UA702A
25 9 2.3.4.5.6.7. 20	Transistor.	MSFC \$38/105	S2N6 97
9, 10, 11, 13, 15, 16			
17.18.19.20.22			
23.24.26			
26 @ 8,12,21,25. 4		MSEC 338/108	\$2 N1132
27 CR 1.2, 3.5, 10, 24		MSFC-338/3	SIN6.26
11, 12, 13, 14, 17,			
	ASSY: USED ON: 49-200-485-501 & 502	501 & 502	
730	UNLESS OTHERWISS NOTED DIMENSIONS ARE IN INCHES & MACHINING TOLENAMORS ARE:		
1 Au (1) Man on or (1) Au (1)	DIMENSIONS UP TO 6 INCL. OVER 6 TO 24 INCL.	OVER 24	BILL OF MATERIAL
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3	OTCIMAL. ±	×	Mob. 10
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24 = 20 A A A A A A A A A A A A A A A A A A	ALLIS-CHALMERS MFG. CO., Milwethee, Wis.		FIGURE 422A
* = = = = = = = = = = = = = = = = = = =		DEPT. SIMILAR TO:	Cont. Co.
7.0 K.	TATO TATE 12-9-65 CHO FOT M. 7/20	2 20	49-200-455-501
			PSP. AGLINAUKER WID. FORM BOSI-4 1-49

	CIRCL		CIRCUIT COMPONENT LIST	T FOR ORA	DRAWING 78-500-187-	103-481
ĮĖĝ	REFERENCE	AEO.	DESCRIPTION		MIL SPEC. OR MFG.	MIL TYPE OR MFG, PART NO.
* 7	18 19 20 23 24					
** A	78 36 27 29 30 37					
	38 39 40 41					
28	CR 28.31.33	m				1N4003
29		2			MSFC-338/8	STN751
30	-				MSFG-338/11	SIN964B
F	6				MSFC 139 P	STN75RA
32	(CR 15 16 35 36				MSFC-338/8	SIN747A
33						IN3034B
3.4.	CR 25, & 7	. N	Zanor Diode		**************************************	SIN968B
ે. 3ક			Refer Lanching 24VDC		Potter & Banmilald	#111DR
	-		Ι.			

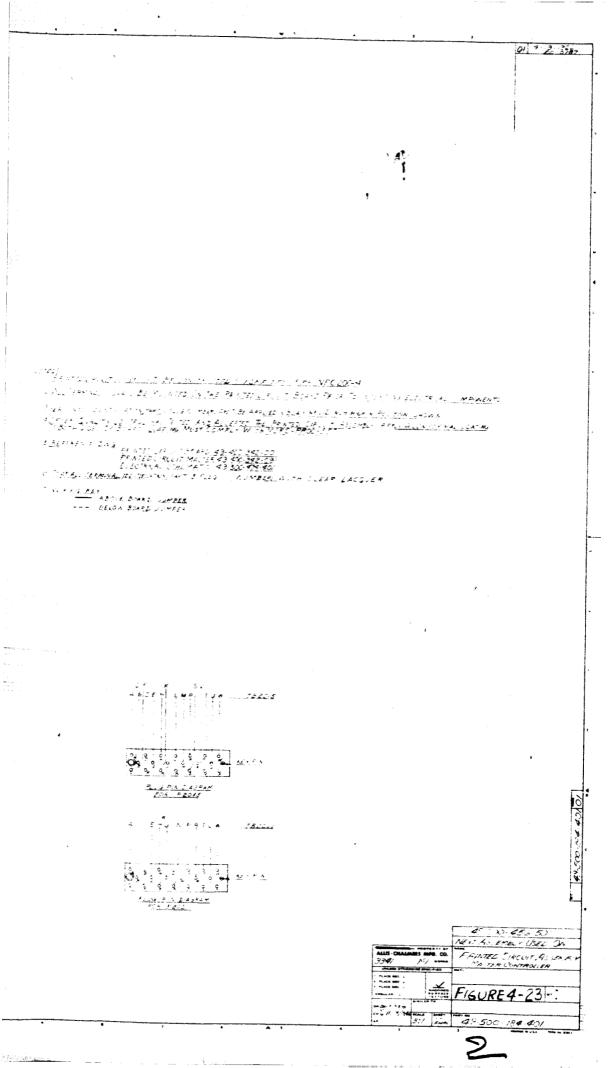
}	F2055 F2021	7	Commercial	Winchestar	SMR F. 20. PCH	
	C20 & G21	~	Capacitor, Ceramic 2200 PF	. MIL-C-11015	CK05CW222K	C
		12	24 Pad Transistor Mounting	TRANSIPAD PRODUCTS LOOIZ DAT. BLACK	LOOIZ DAT. BLACK	1
 			AF: Conductor Solid AWG 24	00-W-343	BELDEN 8022	*
		AR	Shrink Tubing RNF-100.	276-11 7 0D05 Dia.		
	· · · · · · · · · · · · · · · · · · ·	24	Terminal Turret	USECO	20308	- j
		AR	Solder SN60	00.8.571	Type RA	
		AR		MIL-F-14256	Tvn	D l
-		4R	AR WIRE AWG #26 TYPE B	MIL-W-1687211	48.150-009.004	- 1
 			Flectrical Schematic		49:300.474.401	1
╄		N.	SCREW = 2 - 5/1" EG.	MS 5/957	MS51957-14	7
4		X	WASHER, PLAIN	MS15795	MS15 195-804	
+		X	NUT, SELF LOCKING, HEX.	NAS1021	NAS/02/004	
+		AR	LACING TAPE, BLACK	MIL-T- 713A	ALPHA #20134	
┼						E i
4					,	
 						X

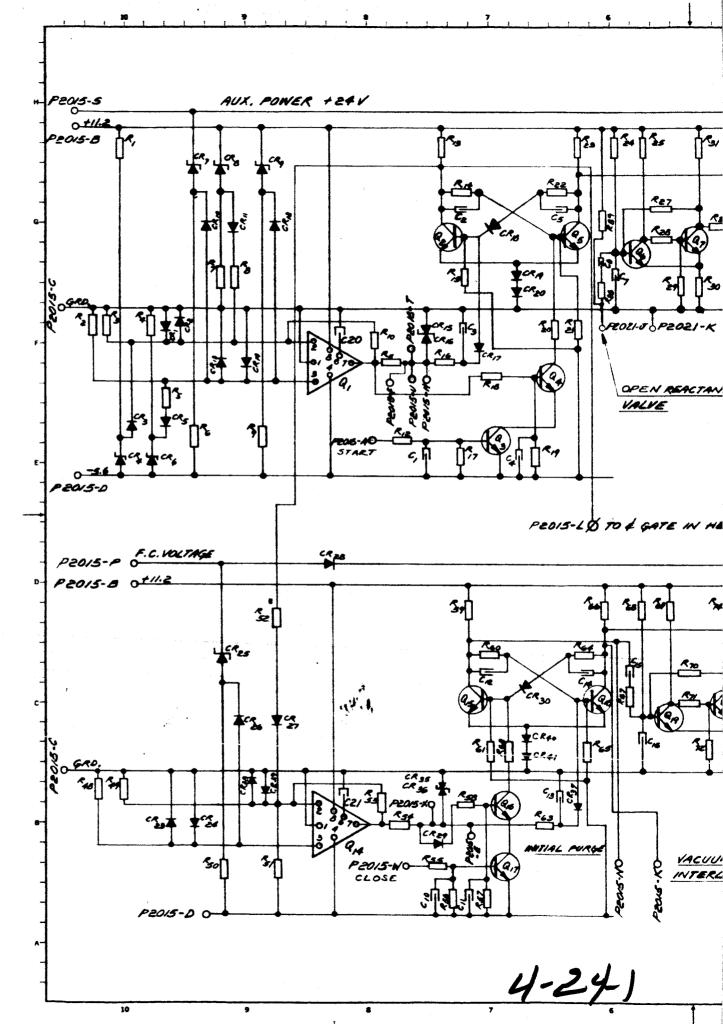
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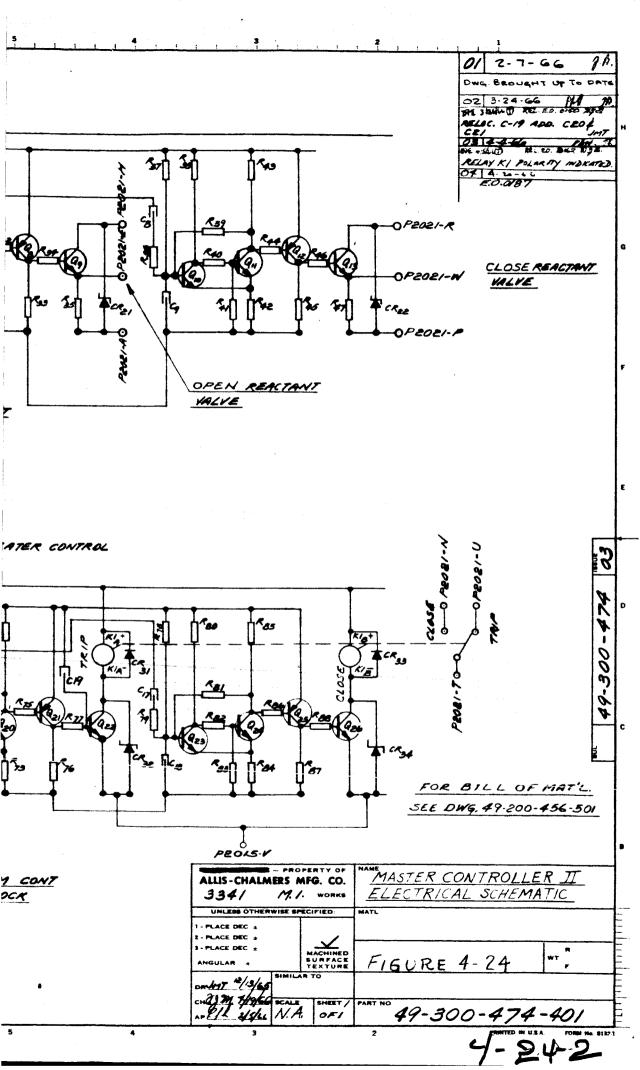
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37. ADDED K	Ker. 004			ALLIS-CHALMERS MFG. CO., Milwaukee, Wis.	CO., Milwaükee, Wis.	10	\$16URE 4-22B
S. 59 THRU DYG NO NO MAS Y	49 ADDED			RESEARCH 3341	[334] DEPT.	SIMILAR TO:	SCALE == 12
0. 018174	H. F.	ъ.		TRD	CHE FJM. 4/20/66	SHEET 2	49-200-456-501
	-	`	ξψ	3.	8 ,	A.C. MIFG CO. M	A-CHING CO. MENNAJKE WIS' FORM SOBES SIN



4-23-1







To apply an external load to the fuel cell, an apply load signal is applied to the load flip-flop providing the start AND gate has been satisfied. This will actuate the load relay, sent a signal to the purge controller initiating a purge cycle, and complete the interlock requirements for the water removal valve (valve cannot be opened unless load has been applied.

The reactant inlet valve is opened manually through the reactant inlet valve driver.

To shut down the fuel cell, a stop signal is applied to stop OR gate. This activates the stop flip-flop which in turn triggers the valve driver to close the reactant valve. At the same time, the same flip-flop triggers the "Main Circuit Breaker OR gate" which trips the "Load Trip Relay" through a flip-flop. Also the stop OR gate deactivates the water cavity pressure controller which closes the moisture removal valve, and interrupts the "OK to heat signal which stops all heating untill the start command is initiated again. The liquid coolant valve will automatically close dependent on temperature. Other inputs such as: High reactant pressure, over-temperature, supply voltage and emergency stop will shut down the fuel cell in an identical manner.

'Trip main circuit command "will trip the load and close the moisture removal valve. Fuel cell voltage less than 21 VDC will trip the load and close the moisture removal valve.

4.6 CANISTER AND SUPPORT SUBSYSTEM

The canister houses the Fuel Cell Stack and Thermal Conditioning and Control Subsystems. Acting as a pressure vessel, it contains and manifolds the helium gas coolant. Brackets bolted to the canister provide a means of rigidly mounting the assembly.

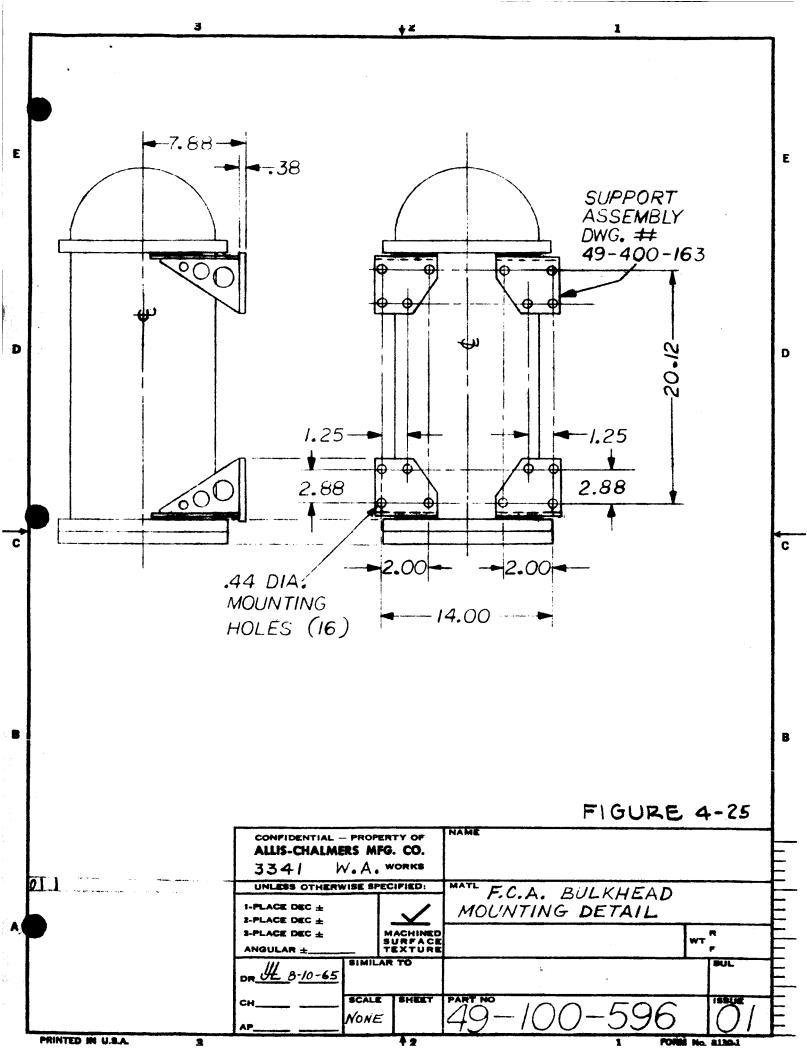
4.6.1 Canister

The canister, composed of a cylindrical flanged shell and end bell, contains the gas coolant at a pressure of 40 ⁺ 2 psia and is designed for a burst pressure of 150 psia and a proof pressure of 100 psia. The canister is fabricated from a magnesium alloy. The cylindrical shell walls are 1/16 inch thick, whereas the spun end bell walls are 3/32 inches thick. Sealing between the cylindrical shell flanges, the end bell, and the fuel cell stack bottom end plate is accomplished with elastomer "O" rings.

Provisions are made on the cylindrical portion of the end bell for entry and return of the liquid coolant as well as entry of electrical blower leads and thermal instrumentation. The bottom end plate has a port provision for the initial charging or depressurization of the gas coolant in the canister. The canister pressure is continually monitored through this port by a 0-50 psia absolute - pressure transducer. A 45 psia relief valve is provided for over pressure protection.

4.6.2 Support

A rigid support is provided by four brackers that mechanically fasten to the flanges of the cylindrical canister shell as shown in Figure 4-25. The



brackets attach to the canister through thermal insulating mounts to minimize losses due to thermal conduction.

The Reactant Control and Conditioning Subsystem is also attached to the canister through thermal insulation mounts, thereby isolating it from the canister, except for the tube connections.

4.7 TEST INSTRUMENTATION

4.7.1 Thermocouple Instrumentation

There are 12 iron-constantan thermocouples located in and outside of the Fuel Cell to permit detailed temperature analysis. (Figure 1-2A and 1-2B (Drawing No. 49-500-125-404), Fuel Cell System Interface Schematic, shows the location of the thermocouples. Figure 2-9, Sheet 5 of 5 NASA Interface Connections) gives the location and function of each thermocouple.